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# Reinforcing carbon fiber epoxy composites with triazine derivatives functionalized graphene oxide modified sizing agent



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# ABSTRACT

To improve the dispersion of graphene oxide (GO) nanosheets in sizing agent and to enhance the interfacial adhesion between GO and epoxy, GO nanosheets were chemically modified with cyanuric chloride (TCT) and diethylenetriamine (DETA). The functionalized GO (i.e. GO-TCT-DETA) with different contents was introduced into the carbon fiber (CF) interface by sizing process. The uniform distribution of GO sheets on CF surface and the enhancement of surface roughness were obtained. Moreover, significant enhancements (i.e., 104.2%, 100.2%, and 78.3%) of interfacial shear strength (IFSS), interlaminar shear strength (ILSS), and flexural properties were achieved in the composites with only 1.0 wt% GO-TCT-DETA sheets introduced in the fiber sizing. The GO-TCT-DETA in the interface region enhanced the stress being transferred effectively and the local stress concentrations being relieved. This study indicates that the utilization of functionalized GO is one of the alternative approaches for controlling the fiber-matrix interface and improving the mechanical properties of CF epoxy composites.

## **1. Introduction**

Carbon fibers (CFs) reinforced polymer composites with high specific strength, great corrosion resistance, light-weight, and favorable design flexibility are superseding the conventional metal and ceramic materials in a variety of high-performance structural and functional applications, such as aerospace, automotive, industries, sports and so on  $[1-13]$  $[1-13]$ . The performance of fiber-reinforced composites highly depends on the fiber-matrix interface, a prominent interface can guarantee the efficient stress transfer from the weaker matrix to the stronger fiber, which is conducive to reduce stress concentrations and to improve overall mechanical properties [\[14](#page-7-0)–16]. However, stress concentration and crack formation in the interfaces can deteriorate the properties of the composites. Consequently, the surface modification of CFs to develop an excellent interphase is pivotal for improving the performance of composites [\[17](#page-8-0)].

Recently, multiscale reinforcement has attracted substantially technical and commercial interests in developing fibers reinforced polymer composites [\[18](#page-8-0)]. The deposition of nanoparticles onto the CF surface enhanced significantly the interfacial performance by availably augmenting the fiber surface area, and facilitating mechanical interlocking and local stiffening at the interface region [19–[25\]](#page-8-0). Many approaches have been reported to attach nanoparticles to the fiber surface including chemical vapor deposition (CVD) [[26\]](#page-8-0), chemical grafting [[27,28](#page-8-0)], electrophoretic deposition (EPD) [[29,30\]](#page-8-0), nanoparticles modified sizing agents etc. Compared with the above reported methods, nanoparticles modified sizing agent possesses unique simplicity and flexibility and is suitable for large-scale industrial production [[31\]](#page-8-0). Additionally, the attachment of nanoparticles onto the CF surface sized with a polymer coating could not only form a connected network structure at the

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interface to restrain the movement of polymer chains and boost mechanical interlocking as well as affinity with matrix for improving the stress transfer, but also protect greatly the fiber surface and improve the tensile strength of fibers [[32\]](#page-8-0). For example, Wu et al. [[33\]](#page-8-0) reported over 46.5% improvement of interlaminar shear strength (ILSS) in a CF/methylphenylsilicone resin (MPSR) composites when the CNTs were introduced in the fiber sizing and the tensile strength of sized CFs showed a slight increase.

In recent years, incorporation of typical two-dimensional graphene or graphene oxide (GO) sheets has been demonstrated to increase the strength of polymer and to improve the interfacial properties of fiber reinforced composites [\[34](#page-8-0)–36]. However, poor dispersion and agglomeration of graphene or GO in media are the great obstacles and causes nano defects in the interface region and only minimal enhancement of interfacial properties was achieved [37–[39\]](#page-8-0). Therefore, efforts to figure out the factors that influence the composites interfacial properties and to achieve superior enhancement in the interfacial strength are significant and urgent targets.

Low-cost diethylenetriamine (DETA) possesses unique polar characteristics with a mixture of primary, secondary amines groups. It can not only react with GO but also be used as curing and toughening agent for epoxy matrix [40–[44](#page-8-0)]. Cyanuric chloride (CTC) has a triazine ring with stable chemical nature and three active reaction sites of chlorine atoms, and can act as a main tree trunk to construct amine dendrimers [[45\]](#page-8-0). Compared with other polymers or natural products  $[46-52]$  $[46-52]$ , this dendritic compound contains a mixture of primary, secondary and tertiary amines groups. Thus, they are interesting from the perspective for providing a range of active sites to react with epoxy resin [\[53](#page-8-0),[54\]](#page-8-0). If GO surface is covalently functionalized by low-cost triazine derivatives with terminal-amine groups, it would provide an ambient path for strong bonding with epoxy matrix and high dispersion in matrix. The effects of triazine derivatives functionalized GO sizing on the interfacial properties of CF/epoxy resin composites have not been reported yet.

In this work, the GO nanosheets were chemically modified with cyanuric chloride (TCT) and diethylenetriamine (DETA) and then dispersed in the fiber sizing agent. The modified sizing agent was directly deposited on the CF surface. The effects of sizing agent containing GO and modified GO on the interfacial microstructure, interfacial adhesion strength, and flexural property of CF composites were studied and discussed in details.

#### **2. Materials and methods**

#### *2.1. Materials*

PAN-based CFs (7 mm in diameter) were bought from Sino steel Jilin Carbon Co., China. Bisphenol A epoxy resins (E51) and liquid aromatic diamine (H-256) were used as matrix and hardening agent. Natural graphite was obtained from Qingdao Tianhe Co., Ltd. Potassium permanganate (KMnO<sub>4</sub>), sodium nitrate (NaNO<sub>3</sub>), triethylamine (TEAE), lithium aluminum hydride (LiAlH4), methylene chloride, TCT and DETA were purchased from Fengxian Tianjin, China (Qigang Rd, Tianjin).  $H<sub>2</sub>O<sub>2</sub>$ , THF,  $H<sub>2</sub>SO<sub>4</sub>$  and HCl were obtained from Tianjin, China. All reagents were analytical grade.

#### *2.2. Chemical functionalization of GO*

GO was prepared using a modified Hummers method [\[43\]](#page-8-0). The aim of chemical functionalization was to produce more amine-containing functional groups on the GO surface. Firstly, GO was impregnated in saturated LiAlH<sub>4</sub>-THF solution for 2 h to obtain GO-OH. Then, TCT and TEAE were added to the mixture containing GO-OH and THF and stirred for 24 h at 70 °C to obtain GO-TCT. Then, the GO-TCT was dispersed in methylene chloride through ultrasonic for 1.5 h. Finally, the hybrid of DETA and NaOH (mass ratio of 1: 2) was appended to the above solution at 80 $\degree$ C and sustained for 12 h [[55\]](#page-8-0) to acquire DETA functionalized

GO-TCT, labeled as GO-TCT-DETA. The grafting course of TCT and DETA onto GO was described in [Fig. 1.](#page-2-0)

#### *2.3. Preparation of sizing agents including GOs and CF/epoxy composites*

Primarily, the commercial CFs were desized in acetone at 80 °C for 48 h to remove the polymer sizing and pollutants [\[55](#page-8-0)], and were defined as untreated CFs. The extracted CFs were conducted with  $AgNO<sub>3</sub>$  $(0.01 \text{ mol/L})/K_2S_2O_8$  (0.1 mol/L) solution at 343 K for 1 h to generate carboxylic groups (CF–COOH). Then, quantitative GO-TCT-DETA was added into epoxy/toluene solution with a GO-TCT-DETA content of 0.1, 0.5, 1.0 and 1.5 wt%, and the hybrid was stirred for 30 min, the sizing resin was maintained constantly at 1.5 wt% in the fiber sizing. The sizing agents including virgin GO were also acquired by the identical way. The CFs were plucked under a traction by a nip roller using a customized small-scale sizing line, then crossed a sizing dip bath including various GOs-processed sizing agents, and by subsequent drying them in a drying oven. The pulling speed of CFs was maintained gently enough to ensure good wetting and to realize the superfluous resin to be eliminated. At last, the sized CFs were conserved in dryer for future use.

The unidirectional prepreg of CFs and epoxy resin (EP) was fit into a mold to prepare composites by using the molding technique, the epoxy resin (E-51) and curing agent (H-256) were uniformly mixed in a mass ratio of 100: 32. Briefly, the composites were fabricated by heating the samples at 90 $\degree$ C for 2 h without pressure, and pressurized to 5 MPa, heating up to 120  $\degree$ C for 2 h, followed by curing at 150  $\degree$ C for 3 h. The CF content in composites was maintained in the range of  $60 \pm 1.5$ %. The whole preparation courses of the sized CFs and CF/epoxy composites are exhibited in [Fig. 2](#page-2-0).

#### *2.4. Characterizations*

The surface structure and chemical composition of functionalized GOs were measured by FTIR spectrophotometer (NEXUS), X-ray photoelectron spectroscopy (XPS, ESCALAB 220i-XL), X-ray diffraction (XRD, DX-2700) and Raman spectrometer (RM2000). The structures and topographic characteristics of functionalized GO were detected by scanning electron microscope (SEM, JSM-7800F) and transmission electron microscopy (TEM, G2F30).

Dynamic contact angle meter (DCAT21, Germany) was carried out to detect the dynamic contact angle of fiber surface. Deionized water and diiodomethane were used as the test liquids. The polar and dispersive components could be obtained through Equation (1):

$$
\gamma_l (1 + \cos \theta) = 2(\gamma_l^p \gamma_j^p)^{\frac{1}{2}} + 2(\gamma_l^d \gamma_j^d)^{\frac{1}{2}} \tag{1}
$$

$$
\gamma_f = \gamma_f^p + \gamma_f^d \tag{2}
$$

where  $\gamma$ <sub>*l*</sub>,  $\gamma$ <sup>*l*</sup></sup> and  $\gamma$ <sup>*p*</sup><sub>*l*</sub> are the surface tension of the test liquid, and its dispersive and polar components, respectively.

The monofilament debonding test (FA620, Japan) was utilized to analyze the interfacial shear strength (IFSS) between the CFs and epoxy resin. The microdroplets were prepared by the mixture of  $E-51$  and  $H-$ 256 at a weight ratio of 100:32. The fiber was pulled out from the cured resin and the value of IFSS was calculated depending on Formula (3):

$$
IFSS = \frac{F}{\pi dl} \tag{3}
$$

where *F* was the recorded load, *d* was the CF diameter, and *l* was the embedded length with resin. The recorded value of IFSS for each group of specimens was averaged from the data of 50 successful measurements.

The interlaminar shear strength (ILSS) of the CFs/epoxy resin composites was analyzed by a three-point short beam shear test according to ASTM [D2344](astm:D2344). The value of ILSS was calculated according to Equation

<span id="page-2-0"></span>

**Fig. 1.** Schematic illustration of GO functionalized with TCT-DETA: (a) Nature graphite, (b) GO, (c) GO-OH, (d) GO-TCT, (e) GO-TCT-DETA.



**Fig. 2.** The diagrammatic drawing of sizing process including GOs and composites preparation.

$$
(4):
$$

$$
ILSS = \frac{3F_{max}}{4bh} \tag{4}
$$

was the width (mm) and *h* was the thickness (mm) of specimen. All the presented results were an average of five specimens.

Flexural tests were carried out by a three-point bending mode and conducted on GT-7000-A2X (Taiwan, China) with a crosshead speed of  $2$  mm min<sup>-1</sup> according to GB/T 9341-2008. The sample size was

where  $F_{\text{max}}$  represents the maximum compression load recorded (N), *b* 

<span id="page-3-0"></span>60 mm  $\times$  6 mm  $\times$  2 mm. All the presented results were an average of five specimens. The value of flexural strength (σ) was calculated according to Formula (5):

$$
\sigma = \frac{3FL}{2bh^2} \tag{5}
$$

where *F* was the maximum load recorded (N), *L* was the sample span (mm), *b* was the width (mm) and *h* was the thickness (mm) of specimen.

The morphology and roughness  $(R<sub>a</sub>)$  of CF surface were tested by atomic force microscopy (AFM, NT-MDT Co., Russia) and field-emission scanning electron microscopy (FESEM, Quanta 200FEG, Japan).

#### **3. Results and discussion**

#### *3.1. Characterizations of the GO*

The GO modified with TCT and DETA was analyzed by FTIR, as displayed in Fig. 3a. For virgin GO, the absorption peaks at 1039, 1608, displayed in Fig. 5d. For virgin GO, the absorption peaks at 1059, 1006,<br>1716 and 3100 cm<sup>-1</sup> were assigned to C-O-C, C=C, C=O and -OH from carboxyl, respectively [[43\]](#page-8-0). In the spectrum of GO-OH, the absorption peak at  $3388 \text{ cm}^{-1}$  was from the O–H strengthening and the intensity of C– –O was decreased greatly, which was due to the reduction of GO by LiAlH<sub>4</sub>. For GO-TCT, two broad peaks at 1714 and  $1568 \text{ cm}^{-1}$  were attributed to the vibration absorption of triazine ring skeleton, and the signal peak at 826  $cm^{-1}$  was assigned to the -C-Cl of TCT, indicating that



**Fig. 3.** FTIR spectra (a), Raman spectra (b), XRD curves (d) and C1s XPS spectra (d) GO, (e) GO-TCT-DETA and N1s XPS spectra of GO-TCT-DETA and TEM and SEM images of (g, i) GO and (h, j) GO-TCT-DETA.

TCT had been grafted onto the GO surface. After grafting DETA, the peak of C–Cl vanished and new peaks at 1650 and 3446  $cm^{-1}$  appeared, attributing to the vibration and stretching of N–H bond. The peaks at 2844 and 2914  $\text{cm}^{-1}$  were assigned to C–H (-CH<sub>2</sub>) from DETA, testifying the reaction between chlorine (Cl) on GO-TCT and amide groups (-NH2) on DETA [[44\]](#page-8-0). Therefore, TCT and DETA had been covalently attached onto the GO surface.

Raman spectroscopy was adopted to further characterize the surface structures of the functionalized GO, as displayed in [Fig. 3b](#page-3-0). The value of  $I_D/I_G$  of virgin GO was 1.74, after TCT modification, the  $I_D/I_G$  value of GO-TCT was reduced to 1.63, which might be because that the stable six heterocyclic rings in TCT had made up for the sp<sup>2</sup> of GO [\[45](#page-8-0)]. The  $I_D/I_G$ value of GO-TCT-DETA increased to 1.68, which was still less than that of GO. The consequences demonstrated that the covalent grafting of triazine derivatives did not severely destroy the GO carbon lattice.

The exfoliation of virgin GO and modified GO was analyzed by XRD, as exhibited in [Fig. 3c](#page-3-0). The peak value of GO at  $10.85^\circ$  reflected that the layer spacing of graphene was 0.82 nm. After modified by TCT-DETA, GO-TCT-DETA displayed a broad diffraction peak at  $8.3^\circ$ , testifying the increased interlayer spacing (1.09 nm). This manifested that the grafted GO nanosheets with triazine derivatives were stacked together by an incompact manner. Furthermore, the inset illustration revealed different volumes for GO and GO-TCT-DETA with the identical weight, which was consistent with the result of XRD, indicating that the interlayer spacing of GO-TCT-DETA was greater than that of GO due to the reaction chains by interspersing among GO layers.

The surface chemical composition of GO and GO-TCT-DETA was determined by XPS, as presented in [Fig. 3d](#page-3-0)–f. For GO, the binding energy (B.E.) of C1s at 284.6 eV and O1s at 531.9 eV appeared and the contents of C and O were 59.61% and 40.39%, respectively. After grafting TCT and DETA, the Cl2p peak at 197.7 eV vanished and the N1s peak at 399.4 eV showed a little increase from 2.18% to 5.30%, which implied the reaction occurred between the chlorine in TCT and amine groups in DETA. The functional groups on the GO surfaces were estimated by the peak fitted C1s and N1s spectra. The C1s spectrum of GO [\(Fig. 3](#page-3-0)d) displayed peaks at 288.6, 286.7 and 285.3 eV, respectively, which were played peaks at 266.6, 266.7 and 265.5 ev, respectively, which were<br>attributed to the O–C=O, C–O–C and C–OH produced on the GO via modified Hummers method. In the case of GO-TCT-DETA ([Fig. 3e](#page-3-0)), the disappearance of C–Cl peak and the improvement of C–N contents testified that TCT and DETA were already adhered onto the GO surface, which was further identified with the results of FTIR and Raman. The chemical reaction of TCT and DETA with GO was further verified by N1s, as exhibited in [Fig. 3](#page-3-0)f. Three extra peaks at 399.6, 398.5 and 398.1 eV appeared and were attributable to primary, secondary and tertiary amine (C–NH2, C–NH and C–N) [\[56](#page-8-0)], which also proved the chemical reaction between DETA and GO-TCT.

The microstructures and topographies of GO and GO-TCT-DETA sheets were observed through TEM and SEM, as revealed in [Fig. 3](#page-3-0)(g-j). The TEM image shows that the GO sheets displayed a diameter of a few micrometers and some wrinkles. After covalent functionalization, the GO-TCT-DETA surface had some ramifications and folds, which were assigned to the triazine derivative chains grafted on the GO. Moreover, it also showed commendable exfoliation and great dispersion, which was in accordance with the XRD results.

The GO surface was slick and homogeneous from [Fig. 3i](#page-3-0), but the accumulation was more serious and formed a three-dimensional layer. While the surface and edge of GO-TCT-DETA displayed more wrinkles ([Fig. 3](#page-3-0)j), which were resulted from the augmented interlayer spacing through grafting branching chains onto the GO surface, and interlayer structure was slacker than that of GO. Two GO sheets could be linked together to produce a crosslinking of the GO layer by DETA with two terminated amine groups [[57\]](#page-8-0). Moreover, the functionalization to GO by triazine derivative did not generate a prominent damage for the  $sp^2$ structures of GO sheets, which was in line with a mild rise in the  $I_D/I_G$ value in Raman analysis as discussed.

# *3.2. Surface topography of CFs*

The CF surface topographies after sizing GO or GO-TCT-DETA with different ratios were observed by SEM and AFM, as shown in [Fig. 4](#page-5-0). It was noted that the shallow grooves on CF surface had been filled up by a layer of resin-containing GO or GO-TCT-DETA, but some big bulges of GO could be observed in [Fig. 4b](#page-5-0), mainly due to the GO agglomeration resulted from the poor dispersibility of GO in the epoxy sizing agent system even at a low concentration (0.5 wt%), this might affect the degree of interfacial enhancement. [Fig. 4](#page-5-0)c–f presents the surface morphologies of CFs sized by sizing agent with different concentrations of GO-TCT-DETA (0.1, 0.5, 1.0 and 1.5 wt%). With increasing the GO-TCT-DETA content from 0.1 to 1.0 wt%, the number of GO-TCT-DETA deposited on CF surface increased, and could cover the entire CF surfaces homogeneously, as seen in [Fig. 4c](#page-5-0)–e. More and more contact points were created and thus enhanced the mechanical interlocking to stiffen the interface of the resulting composites. However, much higher content of GO-TCT-DETA (such as 1.5 wt%) resulted in the agglomeration of GO during the film formation and the nonuniformity on the CF surface ([Fig. 4](#page-5-0)f), which could cause concentrated regional stress and reduced energy dissipation ability, leading to less effective interfacial enhancement of composites.

#### *3.3. Dynamic contact angle (DCA) analysis*

DCA tests were carried out to examine the effects of sizing agent containing GO or GO-TCT-DETA on the surface energy. The results are summarized in [Table 1](#page-5-0). In comparison with untreated CF, the surface free energy of CF-GO 0.5 increased to  $49.22 \text{ mN m}^{-1}$  from  $30.56 \text{ mN m}^{-1}$  owing to the introduced GO sheets with oxygencontaining functional groups and high specific surface area. For CF-GO-TCT-DETA 0.1, the contact angles were found more distinctly decreasing, decreased to 51.98° for polar water and 45.37° for non-polar diiodomethane, respectively. Furthermore, the surface energy, its dispersion and polar components obviously increased compared with CF-GO 0.5, which was resulted from a better dispersion of GO-TCT-DETA on fiber surface and externally introduced amino-terminated groups. Moreover, with increasing the content of GO-TCT-DETA from 0.1 to 1.0 wt%, the surface energy was enhanced evidently from 55.04 mN  $m^{-1}$  for CF-GO-TCT-DETA 0.1–67.78 mN  $m^{-1}$  for CF-GO-TCT-DETA 1.0, however, the increased amplitude of CF-GO-TCT-DETA 1.5 was decreased due to the reduction in polarity groups caused by the agglomeration of excess GO sheets. A higher surface energy could give rise to a superior wettability particularly, which was propitious to the improvement of the interfacial properties of the composites.

# *3.4. Mechanical property evaluation of CF/epoxy composites*

#### *3.4.1. Interfacial property of CF/epoxy composites*

The effect of the sizing layer with GO sheets on the interfacial performance of CF/epoxy composites was examined by IFSS. The results are presented in [Fig. 5.](#page-6-0) The IFSS of CF-GO/epoxy composites (62.2 MPa) had a small increase (25.4%) in comparison with untreated CF/epoxy composites (49.6 MPa). The sizing with GO introduced on the CF surfaces increased the surface roughness and played an important role in enhancing the interfacial strength, but the GO agglomeration and the weak wettability as well as inferior chemical bonding between GO and epoxy resin confined the improvement of IFSS effectively.

For CF-GO-TCT-DETA reinforced resin composites, the GO sheets surrounding the CFs with the help of triazine derivatives contributed to the improvement of IFSS. The IFSS results of CF-GO-TCT-DETA composites were much higher than those of untreated CF and CF-GO composites, especially CF-GO-TCT-DETA1.0 composites yielding an IFSS of 101.3 MPa, which gave rise to a 104.2% and 62.9% improvement in comparison to untreated CF and CF-GO composites. The improvement of IFSS was mainly ascribed to the increased fiber surface area and the

<span id="page-5-0"></span>

**Fig. 4.** SEM images of (a) untreated CFs, (b) CF-GO 0.5, (c) CF-GO-TCT-DETA 0.1, (d) CF-GO-TCT-DETA 0.5, (e) CF-GO-TCT-DETA 1.0 and (f) CF-GO-TCT-DETA 1.5.





enhanced mechanical interlocking of GO with matrix resin [\[58\]](#page-8-0). In addition, the chemical bond reactions of amine groups on functionalized GO surface with CF and epoxy resin also presented a positive effect on the interface of CF composite. When the functionalized GO sheets were distributed uniformly on the CF surface, which was conducive to enhance the stress transfer efficiencies and stiffen effectively at the interface area. Whereas, further increasing the GO-TCT-DETA content to 1.5 wt% led to the reduced IFSS owing to the agglomeration of GO-TCT-DETA in the interface area, as verified by Fig. 4f.

The complex interface layer of CF/epoxy composites might be composed of nanoparticles (GO-TCT-DETA) and sizing polymer (epoxy resin), which could effectively present synergistic effects in the integrated interface region and enhance the interfacial interactions. The failure morphologies of debonding regions were observed by SEM, as illustrated in [Fig. 5](#page-6-0)(a-f). The debonding failure surfaces of untreated CF presented a smooth topography without any residual resin. For CF-GO, a little resin remained on the failure surfaces while a big void appeared between CF and resin in [Fig. 5](#page-6-0)b, this manifested that the GO agglomeration might influence the stress transfer. It was noted that with adding the GO-TCT-DETA in sizing, the debonding failure surfaces became rougher, more and more bulges (epoxy fragments and GO sheets) remained on the surface as seen in [Fig. 5c](#page-6-0)–e. This was because that both interfacial bonding (carboxyl-CFs and amino-GO, amino-GO and epoxy) all became too strong to be pulled-out easily, the schematic diagram of interface reactions was illustrated in [Fig. 5](#page-6-0) (below). Obviously, the GO sheets with good dispersity and chemical activity were highly effective in intensifying the mechanical interlocking and interfacial reaction as well as repressing the crack diffusion at the interface [[59\]](#page-8-0).

The ILSS was further employed to testify the effects of sizing agent with GO and GO-TCT-DETA on the interfacial performances in CF/epoxy composites, as presented in [Fig. 5.](#page-6-0) The ILSS of CF/epoxy composites was increased by 100.2% from 35.6 MPa for untreated CFs without sizing to 71.3 MPa (a maximum ILSS) for CFs with GO-TCT-DETA 1.0 sizing. Compared to CFs sized by GO, the introduction of GO-TCT-DETA has made more contribution to the ILSS. It could conclude that the uniformly dispersed GO sheets on CF surfaces could prominently increase the interfacial interactions. Adding nanosheets would affect the interfacial stress transfer. Zhang et al. [[60\]](#page-8-0) reported a 27.2% improvement of ILSS in a fiber/epoxy composites when GO modified sizing agent was introduced on the CFs surface. Wu et al. [\[27](#page-8-0)] reported that the ILSS of the fiber/methylphenylsilicone resin composites was increased by 46.52% through introducing silanized carbon nanotubes modified sizing agent on the CFs surface. Compared with previous studies, the sizing agent with GO-TCT-DETA on CF reinforced composites had the highest ILSS percentage increased.

## *3.4.2. Flexural property of CF/epoxy composites*

The flexural behaviors were evaluated to further study the comprehensive effects of GO and GO-TCT-DETA sizing on CF/epoxy composites, which could mirror the structural features of the modified laminates in response to complicated stress states. The flexural testing results are shown in [Fig. 6.](#page-6-0) It was clearly demonstrated that the GO and GO derivative attachment endowed the hierarchical composites with a higher flexural strength and modulus than the untreated fiber composites. The increase of GO-TCT-DETA content resulted in a gradual improvement of the flexural strength. The CF-GO-TCT-DETA 1.0/epoxy composites exhibited a maximum flexural strength (1202.0 MPa) and modulus (70.3 GPa), with an increase of 78.3% and 77.5% in comparison with untreated CF composites, respectively. Inversely, a further addition of GO-TCT-DETA led to a reduction of flexural properties. The degeneration in the mechanical performances could be due to the exasperation of GO-TCT-DETA dispersibility in interface area.

Basically, the interfacial failure mode of composite includes adhesive and cohesive failure, which depended on the interfacial states [\[61](#page-8-0)–63] The SEM images in [Fig. 7](#page-7-0) show the fracture morphologies of the composites, revealing a prominent difference between the untreated CF and derived GO-reinforced composites. For untreated CF composites, the interface de-bonding between CFs and epoxy was obvious and the

<span id="page-6-0"></span>

**Fig. 5.** IFSS and ILSS of CF/epoxy composite and SEM micrographs after de-bonding samples: (a) untreated CFs, (b) CF-GO 0.5, (c) CF-GO-TCT-DETA 0.1, (d) CF-GO-TCT-DETA 0.5, (e) CF-GO-TCT-DETA 1.0 and (f) CF-GO-TCT-DETA 1.5 and Schematic diagrams of interface reaction between CF-GO-TCT-DETA and epoxy (below).



**Fig. 6.** Flexural properties of composites: (a) Flexural stress-strain curves, (b) Flexural strength and modulus.

pulled-out fibers representatively presented a smooth fracture surface ([Fig. 7a](#page-7-0)). The fracture micromechanism was seen to be principally adhesive failure and the schematic diagrams were displayed in [Fig. 7d](#page-7-0). While in the CF-GO/epoxy case [\(Fig. 7b](#page-7-0)), the CFs surface was not as clean as that of untreated CFs and the extent of pull out was less. Some resin fragments and GO remaining on the CFs surface were traced, the fiber/epoxy debonding was combined with the fiber pull-out and resin/resin debonding [\(Fig. 7e](#page-7-0)), manifesting the slight improvement of interfacial adhesion after GO modified sizing treatment. For CF-GO-TCT-DETA 1.0 composites ([Fig. 7](#page-7-0)c), the number of de-bonding fiber decreased and the de-bonding took place in the matrix, which indicated the increased interfacial strength and the distribution state of GO-TCT-DETA in the matrix surrounding CFs. The primary mechanism of fiber/matrix debonding was cohesive failure ([Fig. 7f](#page-7-0)). Moreover, the

development of these microstructures would be also related to the enhanced interface layer supplied by GO-TCT-DETA sizing, which was responsible for improving the load transfer between epoxy and CF surfaces [[64,65\]](#page-8-0).

#### **4. Conclusions**

A brief and efficient approach was used to introduce triazine derivatives functionalized GO onto the CFs surface by sizing process for the CFs/epoxy composites. The TCT-DETA was grafted successfully on the GO surface. The dispersion of GO-TCT-DETA in sizing agent was better than that of virgin GO. An epoxy sizing with different contents of GO-TCT-DETA was deposited onto the CFs surface and the surface roughness increased prominently. The addition of GO-TCT-DETA improved

<span id="page-7-0"></span>

Fig. 7. Micro-morphologies and schematic diagrams of interface failure (a,d) untreated CF composite, (b,e) CF-GO 0.5 composite, (c,f) GO-TCT-DETA 0.5 composite.

effectively the covalent bonding, mechanical interlocking and wettability between CFs and matrix. Furthermore, the nanoscale reinforcing interface containing moderate GO-TCT-DETA could enhance effectively the stress transfer and relieve stress concentrations. The composites reinforced with CF-GO-TCT-DETA 1.0 showed the highest enhancement in the interfacial adhesion, increasing 104.2% and 62.9% in IFSS in comparison to that of untreated CF composites and CF-GO composites, respectively. The flexural properties of CF-GO-TCT-DETA modified CF composites, including flexural strength (1202.0 MPa) and modulus (70.3 GPa), are higher than that of the normal composites (674 MPa and 39.6 GPa). The fibers modified by CF-GO-TCT-DETA without agglomeration exert the highest mechanical properties. Therefore, the presented approach shows a potential for enhancing the interfacial and flexural properties of CFs reinforced composites through using functionalized GO sheets modified fiber sizing for many potential applications including electromagnetic interference (EMI) shielding [\[66](#page-8-0)–68], anticorrosion coating [[69\]](#page-9-0), catalysis [[70\]](#page-9-0), energy [71–[73\]](#page-9-0), value-added chemicals from wastes [[74\]](#page-9-0), unique coating [[54,](#page-8-0)[75\]](#page-9-0), and potential electronics [\[76,77](#page-9-0)].

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