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8

9 Abstract

10 Wood/epoxy resin composites based on diglycidyl ether of bisphenol A (DGEBA)/epoxidized oil 11 (EO)/Diels-Alder adducts of resin acids with maleic anhydride (RAMA) in acetone (80 %) were obtained by 12 impregnation. Epoxidation was carried out in the presence of hydrogen peroxide (H₂O₂), acetic acid (AAc), 13 sulfuric acid (H_2SO_4) as catalyst and cyclohexane (CHx) as solvent at a molar ratio of 0.5/1.5/114 (AAc/hydrogen peroxide/ethylene unsaturation). The kinetic parameters (activation energy and pre-15 exponential factor) of the DGEBA/EO/RAMA curing reaction and thermal characterization of the 16 crosslinked compounds and wood epoxy composites (WECs) were obtained using differential scanning 17 calorimetry (DSC) and thermogravimetric analysis (TGA). Based on the chemical structure of the evolved 18 gases resulted during thermal decomposition of the crosslinked polymers and WECs, identified with FT-IR, 19 a probable mechanism of thermal degradation was proposed. Resistance to three fungi was also tested. 20 21 Keywords: Wood, Thermosetting resin, Cure behaviour, Thermal properties, Biological resistance

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1 1. Introduction

Nowadays, composites based on natural materials are widely used in industrial and household fields,
because they are environmentally friendly and originate from renewable resources. Wood is among the most
important renewable resources. It has a great importance for life sustainability, as well as both raw and
processed material. The most important components of wood are lignin, cellulose, hemicelluloses and resins.
Under environmental factors influence (i.e. temperature, light, moisture, microorganisms, insects, etc.), there
occurs wood damage, followed by a decrease in technical (thermal, mechanical and electrical behaviour) and
aesthetic aspects [1, 2].

9 To preserve the properties of wood, physical and chemical methods, including heat treatment, 10 chemical modification, impregnation and physical coatings, have been used. Considering its chemical 11 structure (mainly hydroxyl groups), wood was modified by esterification and etherification reactions with 12 anhydrides, acids, acid chlorides, epoxy resins, unsaturated derivatives, cyclic ethers, lactones, alkyl 13 chlorides and so on. These transformations were aimed to improve mechanical and electrical properties, as 14 well as to enhance resistance to environmental factors action [3–13].

15 Vegetable oils (edible or non-edible) are a renewable source of raw materials, mainly esters of 16 glycerol, which are the result of glycerol esterification with three saturated and/or unsaturated fatty acids [14]. 17 As a consequence of the chemical structures, these oils may be modified to obtain new monomers that can 18 induce special properties in the final polymers (flexibility, biocompatibility, biodegradability, thermal 19 stability) [4, 15–20]. Hemp oil and flax oil, as non-edible oils that contain a large number of unsaturated 20 groups in their structure, represent an excellent source of raw material for the synthesis of monomers with 21 new functional groups capable to polymerize. One of the most common methods of chemical modification of 22 vegetable oils is epoxidation. Epoxidized oils may be used as basis for their transformation in acrylated, 23 methacrylated, hydroxylated monomers, used either individually or mixed in various polymeric compositions 24 [16, 17, 21–25]. Also, vegetable oils and their derivatives, alone or in combination with various fungicides, 25 have been used to increase the decay resistance of wood [26, 27].

Rosin is a renewable naturally raw material consisting of neutral compounds (turpentine) and resin acids (abietic, levopimaric, neoabietic, palustric, fatty acids, etc.). As a consequence of their chemical structure, the resin acids can be converted into several types of monomers. In particular, the most common transformation is the Diels–Alder reaction, when some polyacids are obtained and further used as

crosslinking agents for epoxy resins [28–35]. These adducts, through their chemical structure, may improve
 the properties of the crosslinked epoxy resins.

Epoxy resins are some of the most widely available synthetic monomers, which, after curing, present excellent electrical, mechanical and thermal properties in a vast palette of application fields, although not being environmentally friendly [36, 37]. This behaviour depends on the formulation, chemical composition and crosslinking conditions. By using some natural ingredients (rosin acids and vegetable oil derivatives), these formulations may compensate some drawbacks and be environmentally friendly [16, 20, 28–35, 38, 39].

9 The paper describes the curing and non-isothermal degradation kinetics of compositions based on 10 DGEBA/EO/RAMA and WECs. The novelty of the work consists in the using of some epoxy resins based 11 on vegetable oils and of a curing agent derived from resinic acids of natural origin. Also, the thermal and 12 fungal resistance properties were followed using DSC and TG analyses. Based on FT–IR analysis of the 13 evolved gases during thermal decomposition a possible degradation mechanism is proposed.

14

15 2. Experimental

16 2.1. Materials

17 Hydrogen peroxide (H₂O₂), glacial acetic acid (AAc), maleic anhydride (MA), potassium hydroxide 18 (KOH), sulfuric acid (H₂SO₄), triethylbenzylammonium chloride (TEBAC) and anhydrous sodium sulfate 19 (Na_2SO_4) were analytical grade products and used without any purification. The solvents were used as 20 received or distilled before use. Resin acids (RA) were obtained from commercial rosin by acid 21 isomerization and by repeated recrystallizations from concentrated acetone solutions and had an acid number 22 (a. n.) of 181 mg KOH g⁻¹ and melting point (m. p.) of 161 °C [33]. RAMA with m. p. 230 °C and a. n. 434 23 mg KOH g^{-1} was obtained following a procedure described in the literature [40]. DGEBA, a commercial 24 product (Sintofarm, Romania), (average epoxy equivalent weight of 190 g eq⁻¹, viscosity of 12000 mPas at 25 25 °C) was used as received. Flax oil (FO) and hemp oil (HO) have been obtained from the local market and 26 have the following compositions supplied by the manufacturers: flax oil [saturated fats 10.1 wt. %, 27 unsaturated fats (oleic acid 22.4 wt. %, linoleic acid 14.3 wt. %, α-linolenic acid 52.3 wt. %), other acids 0.9 28 wt. %] and hemp oil [saturated fats 8 wt. %, unsaturated fats (oleic acid 11.4 wt. %, linoleic acid 57 wt. %, 29 α -linolenic acid 18.7 wt. %, other acids 2.9 wt. %)]. Epoxidized flax oil (EFO) (number of epoxy groups 5.9 30 mol^{-1}) was obtained as described below and epoxidized hemp oil (EHO) (number of epoxy group 3.5 mol^{-1})

1 was obtained following a procedure described in the literature [23]. The number of epoxy groups was 2 measured using ¹H–NMR spectroscopy. The softwood samples (W) (*Abies alba L.*) had the same 3 characteristics as those presented in a previous work [9].

4

5 2.2. Sample preparation for DSC and TGA studies

For the DSC studies, the formulation DGEBA/EO/RAMA at a molar ratio of 0.8/0.2/0.66 (epoxy
ring/carboxyl proton 1/1) in the presence of TEBAC as catalyst was prepared. After a vigorous mixing of the
reactants, they were degassed in a vacuum oven at room temperature and a portion has been stored at 0 °C
before the DSC recording was performed. The DGEBA/EO/RAMA compositions used for the TG
characterization were transferred in an aluminum form and crosslinked according to the following protocol: 1
h at 100 °C, 1 h at 135 °C and post cured 4 h at 185 °C (Scheme 1).

12

Scheme 1

The WEC samples were obtained by immersion of W samples for 8 h in the next formulation: DGEBA/EO/RAMA at molar ratio 0.8/0.2/0.66, 80 wt. % solution in acetone, in the presence of TEBAC as catalyst. After immersion, the impregnated samples were placed in a vacuum oven at 40 °C and maintained another 8 h to release the solvent. Then, the WECs were cured at 70 °C for 1 h, 1 h at 100 °C, 1 h at 135 °C and then post cured at 150 °C for 3 h and used for TGA studies. The same samples were also used for crystallinity measurements and for morphological analysis. The weight fraction of W in WECs was 90 %.

19

20 2.3. Measurements and methods

The acid number (a.n.) was obtained using a slightly modified ASTM D 465–05. The sample dissolved in acetone at 10 % (w/v) concentration was titrated with 0.5 N ethanolic KOH solutions in the presence of phenolphthalein as indicator [35, 41]. The epoxy equivalent weights (EEW) were obtained using ASTM D 1652–04 [42]. The number of the double bonds from oils was obtained using ¹H–NMR spectroscopy, with the next equation [43]:

26

$$D_{b} = 0.5(A - N_{f}) / N_{f}$$
(1)

27 where: D_b is double bonds number, the A is the surface 28 assigned to the olefinic protons located between 5.2 and 5.4 ppm and $N_{\rm f}$ is the normalization factor (obtained 29 through the dividing by 4 of the protons area from 4.0 and 4.3 ppm assigned to terminal protons of glycerol).

The melting points were obtained with a DSC 200 F3 Maia device (Netzsch, Germany), at 10 °C min⁻¹
heating rate.

FT-IR spectra were acquired with a Vertex 70 apparatus (Bruker–Germany) using KBr pellets. ¹H–NMR
spectra of DGEBA, oils, epoxidized oils and RAMA were recorded with an Avance DRX 400 (Bruker–
Germany) apparatus at 50 °C using CDCl₃ and DMSO–d₆ as solvents and tetramethylsilane (TMS) as
internal standard.

7 TG curves were recorded in the temperature range 30–600 °C, in inert atmosphere (N₂ flow rate of 40 mL 8 min⁻¹) at three heating rates (10, 20 and 30 °C min⁻¹) using STA 449 F1 Jupiter device (Netzsch–Germany). 9 Open Al₂O₃ crucibles were loaded with approximately 10 mg of the ground sample. Gaseous products 10 resulting from thermal degradation were transferred through a transferring line made from Teflon, coupled to 11 the head of the TG balance, with 1 m length and with 1.5 mm diameter (heated at 190 °C to limit 12 condensation) to the FTIR apparatus having a MCT detector (Mercury Cadmium Telluride). The FT-IR spectra were recorded between 4000 and 500 cm⁻¹ wavenumber values and processed with OPUS 6.5 13 14 software.

DSC analysis was undertaken on a DSC 200 F3 Maia apparatus (Netzsch, Germany), under nitrogen flow rate of 50 mL min⁻¹, at three heating rates (5, 10 and 15 °C min⁻¹) in the temperature range 25–300 °C. The calibration of the apparatus was made with high purity indium. The samples weighing up to 10 mg were placed in aluminum cells provided with a pierced lid, were scanned in the presence of one aluminum empty cell as standard. The heat flow versus temperature was recorded. DSC data were recorded consecutively using the same sample on the same day [44].

The evaluation of the kinetic parameters, both for curing and thermal degradation reactions were obtained using DSC and TG scans and processed with Netzsch Thermokinetics 3 software [45]. In a first instance, these parameters were evaluated on the basis of free–estimation methods of Ozawa–Flynn–Wall (OFW) and Friedman (FD). The used equations are as follows [46–48].

$$\ln\beta = C - 1.052(E_O/RT_p) \qquad (OFW \text{ equation}) \qquad (2)$$

26 and

27
$$\ln\left(\frac{d\alpha}{dT}\right) = \ln\left(\frac{A}{\beta}\right) + \ln(f(\alpha)) - \frac{E_{FD}}{RT}$$
 (FD equation) (3)

1 where: *A* is the frequency factor, β is the heating rate, *C* is a constant, E_O and E_{FD} are the specific activation 2 energies of reactions obtained with OFW and FD relations, T_p is the exothermic peak temperature in Kelvin 3 and *R* is universal gas constant.

These methods, included in "Netzsch Thermokinetics 3", a software module for the kinetic analysis of thermal measurements, permit the evaluation of the kinetic parameters and the variation of activation energy values versus conversion degree, without assuming any reaction model. Changes in the shape of the activation energy versus the degree of conversion curves indicate that the degradation reactions occur following a complex mechanism in several independent stages through consecutive, parallel or competitive processes [49, 50]. This makes it possible to choose between different mechanisms and obtain a global model that gives the best results for the curing or thermal degradation processes.

Morphological study of WECs was conducted by analyzing the scanning electron microscopy (SEM) images. These were obtained using the SEM/ESEM-EDAX-QUANTA 200 apparatus which operated in the following parameters: field emission filament 16 kV accelerating voltage, high vacum mode and maximum magnification of 5000 X. The images were obtained on the surface samples, cut perpendicularly on the sense of growth and gilded to make them conductive.

16 Anti-decay resistance testing was performed on untreated wood (blank), polymer and WECs. The test 17 samples were obtained as previously described above. The main components of wood (cellulose, 18 hemicelluloses, lignin), under favorable conditions of humidity and temperature, can be metabolized by fungi 19 as nutrients, resulting in wood degradation. Four samples from each specimen, dried to constant weight at 20 105 °C, were tested in the same conditions for resistance against decay. The following fungi were used: a 21 white rot fungus Penicillium chrysogenum ATCC10106 (P. chrysogenum), a brown rot fungus Cladosporium 22 cladosporioides ATCC16022 (C. cladosporioides) and black rot fungus Aspergillus brasiliensis ATCC 9642 23 (A. brasiliensis). The samples were placed in Petri dishes on a substrate of malt extract (for P. chrysogenum) 24 and potato dextrose (for C. cladosporioides and A. brasiliensis) in agar which were previously inoculated 25 with a standard inoculum of 0.5 McFerland for each fungal strain. All the Petri dishes were incubated at the 26 room temperature $(24 \pm 1 \text{ °C})$ for 10 weeks. The fungal growth on the untreated and treated samples was 27 monitored during the 10 weeks of incubation and at the end of the experiment the wood samples were 28 removed from the culture plates and the fungal biomass was gently removed with the aid of a wet cotton 29 fabric. The wet samples were oven-dried at 105 °C, in order to reach constant weight. Then all the samples 30 were accurately weighed in order to notice the retained moisture.

1	Crystallinity of W and WECs was measured with the aid of wide angle X-ray diffractometry (WAXD).The
2	WAXD curves were recorded using a Bruker D8 Advance (Germany) apparatus with CuK_{α} monochromatic
3	radiation ($\lambda = 0.15406$ nm) at 25 °C, 36 kV and 25 mA, in the interval 2 θ diffraction angles (Bragg angle)
4	ranging between 4 and 40 $^{\circ}$.
5	The crystallinity index was calculated using the next equation [51]:
6	$I_{\rm c} (\%) = [(I_{002} - I_{\rm am})/I_{002}] \cdot 100 $ (4)
7	where: I_c is crystallinity index, I_{002} is maximum value of intensity at the 002 crystalline peak, I_{am} is the
8	maximum value of amorphous peak intensity [52].
9	The polymer weight percentage gain (WPG) after crosslinking was calculated with the next equation:
10	WPG (%) = $[(M_f - M_i)/M_f] \cdot 100$ (5)
11	where: M_i is the initial weight of W and M_f is the final weight of WEC sample after crosslinking.
12	The humidity values after fungal attack were calculated as follows:
13	H (%) = $[(M_w - M_d)/M_w] \cdot 100$ (6)
14	where: H is the percent of the humidity; M_w is the weight of wet sample after fungal attack and M_d is the
15	weight of the same sample after drying.
16	The weight losses (WL) (%), after the fungus attack were calculated with the equation:
17	WL (%) = $[(M_i - M_d)/M_i] \cdot 100$ (7)
18	where : M_i is the weight of initial sample before fungal attack and M_d is the weight of the same dried sample
19	after fungal attack.
20	Twenty two solvents with solubility parameters (δ) between 7.24 up to 23.5 cal cm ⁻³ were used to obtain the
21	swelling parameter of the crosslinked polymers (Table 1). Each solvent used in the study was introduced in
22	Erlenmeyer flasks equipped with plunger stoppers. Over each solvent, polymer samples with a weight of up
23	to 0.1 g were added, maintaining the constant temperature (25 °C) for a long period of time. The weight of
24	the swollen samples was measured until it was stabilized. The swelling degree was calculated with the
25	following equation [53]:
26	Q (%) = $[(M_w - M_i)/M_i] \cdot 100$ (8)
27	where: Q is the swelling coefficient, M_w is the weight of the swollen sample and M_i is the weight of the initial
28	sample.
29	Table 1
30	Fig. 1_revised

1 The solubility parameter of the crosslinked samples is obtained by observing the maximum of the swelling 2 coefficient (Q) in the Q versus δ plot (Fig.1). As it may be seen from Fig. 1, the maximum value is reached 3 for methylene chloride, which is the solvent that induces the highest degree of network swelling. It can be 4 considered that the solubility parameter of methylene chloride, of 9.93 (cal cm⁻³)^{0.5}, may be attributed to the 5 polymer–solvent interaction parameter of the crosslinked polymers. The molecular weight between two 6 crosslinking points (Mc) and the crosslinking density (n) of DGEBA/EO/RAMA samples were obtained 7 based on the swelling measurements and calculated with Flory–Rehner equation [54]:

8
$$n = -[\ln(1-V) + V + \chi \bullet V^2] / V_{mol}[V^{0.33} - V / 2]$$
(9)

9 where: *V* is the volume fraction of polymer in swollen polymer, V_{mol} is the molar volume of the solvent and 10 χ is the Flory solvent–polymer interaction parameter. The interaction parameter may be obtained with the 11 equation:

12
$$\chi = \frac{V}{RT} (\delta_p - \delta_s)^2$$
(10)

13 where: *R* is the gas constant, *T* is temperature in Kelvin, *V* is the molar volume of the solvent, δ_p is 14 solubility parameter of polymer and δ_s is solubility parameter of solvent.

15

16 **3. Results and discussion**

17 3.1. Synthesis and characterization of epoxidized flax oil (EFO)

18 Into a 0.5 L four-necked reaction vessel placed in a water bath, equipped with mechanical stirrer, 19 thermometer, a water reflux condenser and dropping funnel, 150 g FO, 120 g AAc, 2 mL H₂SO₄ (diluted in 4 20 mL of distilled water) and 40 mL CHx were introduced. CHx was used to reduce the viscosity of the mixture 21 and to minimize the epoxy cycle opening. The reaction mixture was moderately stirred for about 30 minutes, 22 purged with a slow flow of nitrogen and the water bath was cooled with ice to 10 °C. After 1 h, 220 g H_2O_2 23 30 % (w/w) was added in small portions under vigorous stirring, while maintaining the reaction mixture 24 temperature at about 15 °C. After adding the entire amount of H₂O₂, the temperature of the reaction mixture 25 was slowly raised to 55 °C and maintained at this level for another 6 h. For finishing the reaction, the 26 mixture was heated to 65 °C for another 0.5 h and then cooled rapidly on ice water bath. The reaction mass 27 was washed twice with distilled water at 35 °C and then with a 5 wt. % potassium carbonate solution until 28 complete neutralization. Then, the water layer was discharged and EFO was kept on anhydrous sodium

1	sulfate to remove traces of water. Sodium sulfate was removed by filtration and CHx was removed at 60 $^\circ$ C
2	in a rotary evaporator under vacuum. The final product was introduced in a polyethylene vessel and stored in
3	the dark at 20 °C (Scheme 2).
4	Scheme 2
5	The obtained EFO was a low viscosity yellowish color liquid. Its chemical structure was confirmed
6	using FT-IR and ¹ H-NMR spectroscopy analysis. Since there are no significant differences between the FT-
7	IR spectra of the two oils, only the spectra of flax oil and epoxidized flax oil are shown in Fig. 2. The main
8	signals are: 3470 cm ⁻¹ (OH stretching from opened epoxy ring), 2921 and 2859 cm ⁻¹ (CH ₃ , CH ₂ , CH
9	stretching vibrations from fatty acids moieties), 1742 cm ⁻¹ (CO stretching in ester groups), 1455 cm ⁻¹ (CH
10	aliphatic), 1242 and 1157 cm ⁻¹ (C–O–C ester linkages) and 823 cm ⁻¹ (oxirane rings). The signals from 3010
11	cm ⁻¹ and 1654 cm ⁻¹ from FO (specific to the olefin double bond) disappear and a new signal appears at 823
12	cm ⁻¹ specific to the epoxide groups from epoxidized oils (Fig. 2b). ¹ H-NMR spectra of FO and EFO are
13	presented in Fig. 3. The main signals are: 5.182 (the proton located at the secondary C of glycerol), 4.130 -
14	4.290 (glycerol protons), 2.805 - 3.091 (epoxy group protons), 2.28 (methylene protons adjacent to ester
15	groups), 1.25 - 1.47 (methylene protons); 0.85 - 0.92 (methyl protons). The main difference which appears
16	between the ¹ H–NMR spectra of FO and EFO is the absence of the olefinic protons located near 5.35 ppm
17	and presence of the protons attached to the epoxy ring with the peaks located at 2.770 and 3.091 ppm
18	chemical shift.
19	Fig. 2_revised
20	Fig. 3_revised
21	
22	3.2. FT–IR characterization of crosslinked polymers and WECs
23	In Fig. 4 there are presented the FT-IR spectra of W, crosslinked DGEBA/EFO/RAMA and WECs.
24	As it may be observed in the DGEBA/EFO/RAMA and WECs spectra, they do not show any signal specific
25	to the epoxy rings (at 915 cm ⁻¹ for DGEBA and at 823 cm ⁻¹ for EFO), confirming the reaction between the
26	epoxy and carboxyl groups from RAMA. As a result of this reaction, a number of new hydroxyl groups are
27	generated. Their corresponding signals are located at 3346 cm ⁻¹ in the WEC spectrum (Fig. 4c) and overlap
28	with the signal from 3343 cm ⁻¹ specific to wood (Fig. 4a). Also, due to the above reaction, new ester groups
29	appear, which are highlighted by the signal at 1724 cm ⁻¹ (C=O stretching vibrations) and signals from 1234

30 cm⁻¹ and 1028 cm⁻¹ (C–O–C stretching vibrations) (Figs 4b and 4c). There may also be observed a series of

1	signals located near 1606 and 1509 cm ⁻¹ , specific to skeletal vibrations of aromatic entities from DGEBA
2	(Figs 4b and 4c).
3	Fig. 4_revised
4	
5	3.3. Crosslinking density measurements
6	The crosslinking density (n) and the molecular weight between two crosslinking points (Mc) of
7	DGEBA/EO/RAMA networks were determined using swelling measurements and a method described in the
8	literature [54]. Based on the data from Fig. 1, the solubility parameter of methylene chloride [9.93 (cal cm ⁻³)
9	^{0.5}] can be assigned as the polymer-solvent interaction parameter of the two crosslinked polymers. The
10	following values were obtained: $n = 2.065 \ 10^{-3} \text{ mol cm}^{-3}$ and $Mc = 591 \text{ g mol}^{-1}$ for DGEBA/EHO/RAMA
11	sample and $n = 1.862 \ 10^{-3} \text{ mol cm}^{-3}$ and $Mc = 633 \text{ g mol}^{-1}$ for DGEBA/EFO/RAMA. These values of Mc are
12	quite close to the theoretical ones, suggesting a random distribution of the epoxidized oil molecules in the
13	crosslinked polymer structure. The lowest value of Mc for DGEBA/EHO/RAMA sample is due to the
14	smaller number of epoxy groups from EHO, fact which leads to a smaller degree of network packaging. The
15	obtained networks have relative low T_g values (31 °C for DGEBA/EHO/RAMA and 32 °C for
16	DGEBA/EFO/RAMA), as a consequence of internal plasticizing effect introduced by epoxy oils.
17	
18	3.4. Curing of DGEBA/EO with RAMA
19	The obtained DGEBA/EO/RAMA samples (epoxy ring/carboxyl proton 1/1) were crosslinked in the
20	DSC device at three heating rates. In Scheme 1 the chemical reactions between carboxyl and the epoxy
21	groups from DGEBA/EO/RAMA are presented. Since the main reagents in these formulations have more
22	than two reactive groups, with time and temperature increase, three-dimensional networks were obtained. As
23	one may see from Fig. 5a (DSC curves for DGEBA/EFO/RAMA), with the increase in temperature, besides
24	the main peak, a smaller sized peak appears, suggesting that few of the EFO epoxy groups (which have 6
25	epoxy groups) are partially sterically hindered, these groups further reacting with temperature increase. In the
26	case of DGEBA/EHO/RAMA (Fig. 5b), the DSC curves show the same trend at 5 °C min ⁻¹ , while the records
27	at high speeds, present only an exothermic peak, suggesting that all chemical reactions occur simultaneously.
28	The evaluation of the kinetic parameters of the crosslinking reactions (apparent activation energy and
29	preexponential factor) of the above samples was undertaken using the Friedman (FD) and Ozawa (OZ)

Fig	5	revised	
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2	If the curves shapes of apparent activation energy as a function of conversion factor show deviations from
3	linearity, this fact suggests that the crosslinking takes place in several steps (maybe consist of a series of
4	successive or parallel processes) and occur following a complex mechanism [49, 50]. From Figs. 6a and b, it
5	may be observed that the apparent activation energy curves present few maximum and minimum values and
6	depend on the chemical composition of the samples. This suggests that in order to establish the mechanism
7	of the crosslinking process it is necessary for the evaluation to be done using the non-linear regression
8	method (MLR) within the "Thermokinetics 3" software. Based on the initial values of the kinetic parameters
9	obtained with the FD method and the shape of the DSC curves recorded at three heating rates, the software
10	solves numerically the differential equations specific to 18 reaction types, adjusting the theoretical models to
11	registered data. Following the processing of data by the software in the 0.1 to 0.9 conversion degree (α)
12	interval, a three step kinetic model with successive reactions for the DGEBA/EFO/RAMA sample and a two
13	steps model with successive reactions for the DGEBA/EHO/RAMA sample were chosen. The choice of
14	these models was made using the difference between measured and calculated values, on the basis of the F-
15	test and the best correlation coefficient between data.
16	The next conversion functions were used:
17	$ n^{\text{th}}$ reaction order of the autocatalytic model, Cn:
18	$f(\alpha) = (1 - \alpha)^{n} (1 + K_{cat} \cdot \alpha) $ (11)
19	where: K_{cat} is the autocatalytic constant, <i>n</i> is the reaction order
20	- reaction order model, Fn:
21	$f(\alpha) = (1 - \alpha)^n \tag{12}$
22	where <i>n</i> is the reaction order and α is the conversion degree,
23	and
24	 Avrami–Erofeev reaction model, An:
	<u>n-1</u>
25	$f(\alpha) = n(1-\alpha)[-\ln(1-\alpha)]^{-n} $ (13)
26	where <i>n</i> is a constant parameter.
27	The following mechanisms of curing reactions were used:
28	- mechanism coded t:f,f; CnB,Fn,An; for formal kinetic model of A-1 \rightarrow B-2 \rightarrow C-3 \rightarrow D type for
29	DGEBA/EFO/RAMA
30	and

1	– mechanism coded d:f; CnB,Fn; for formal kinetic model of A-1 \rightarrow B-2 \rightarrow C type for
2	DGEBA/EHO/RAMA
3	where: for DGEBA/EFO/RAMA sample, A is the initial reactant; B and C are the intermediate products and
4	D is the final crosslinked resin,
5	and for DGEBA/EHO/RAMA sample, A is the initial reactant; B is the intermediate product and C is the
6	final crosslinked resin.
7	The above codes are specific to "Thermokinetics 3" software (d:f; and t:f,f; represent reaction codes in two
8	or three successive steps, while 1, 2, 3 denote the code for reaction steps). The results obtained from the
9	above samples are showed in Table S1 (See Supporting Information). Using the data from Table S1 and the
10	software, the DSC curves were recalculated. It can be seen that in the temperature range for which the
11	calculations were performed, there is a good correlation between the experimental and the calculated data,
12	which suggests that the proposed crosslinking mechanisms approximate well the real phenomenon. By
13	comparing the data in Table S1, it can be seen that the values of the activation energies for
14	DGEBA/EFO/RAMA are somewhat lower than those for DGEBA/EHO/RAMA. This fact can be explained
15	on the basis of the different chemical structures of the two epoxy oils, EFO having several more epoxy
16	groups than EHO, so the crosslinking reactions occur more easily.
17	Fig. 6_revised
18	
19	3.5. Thermal degradation of the cured products and WECs
20	The chemical structure of the crosslinked polymers are presented in Scheme 1. In Fig. 7a there are
21	given the TG and DTA curves of DGEBA/EFO/RAMA, obtained at three heating rates in nitrogen
22	atmosphere. From Fig. 7a, the main degradation parameters (T_{onset} , T_{peak} , T_{10} , T_{20} , T_{50} and W_{600}) are extracted
23	and summarized in Table 2. Thermograms are very similar for both samples and the thermal parameters also.
24	It can be noted that both polymers exhibit good thermal stability, mass losses being insignificant up to 350
25	°C. The kinetic parameters of the thermal degradation reaction (apparent activation energy and pre-
26	exponential factor) were obtained using MLR. As it can be seen from Fig. 7b, the variation of the activation
27	energy versus the conversion function degree presents a few minima and maxima, which suggests that the
28	thermal degradation process occurs in at least two degradation steps [49, 50].
29	In a range of 0.1 to 0.9 of conversion degree, the MLR method fitted the experimental data to curve shapes

0	Fig. 7_revised
9	around 20.
8	323 kJ mol ⁻¹ for DGEBA/EHO/RAMA sample, while the log A/s ⁻¹ factor has similar values for both samples
7	the chemical structure of epoxy oil and have a value of 302 kJ mol ⁻¹ for DGEBA/EFO/RAMA sample and of
6	Table S2 (See Supporting Information). The activation energies for the first stage of degradation depend on
5	The choice of the optimal model was made on the basis of the criteria presented above and are shown in
4	reactions) which show that thermal degradation occurs through successive processes in two and three steps.
3	$1 \rightarrow B-2 \rightarrow C$ coded as d:f; (consecutive reactions) and A-1 $\rightarrow B-2 \rightarrow C-3 \rightarrow D$ coded as t:f,f; (consecutive
2	performed for several reaction schemes, taking into consideration the formal kinetic reaction model: A-
1	degradation. The Avrami-Erofeev and n th reaction models were used (Eqs. 12 and 13). Calculations were

10

11

Table 2

Using the data from Table S2 the TG curves were recalculated. Good overlapping of experimental andcalculated data curves may be observed (Fig. 7a).

14 In the case of WECs, the thermal characterization was obtained with same software. Fig. 8a 15 presents the TG and DTA curves of W/DGEBA/EHO/RAMA sample obtained at three heating rates in 16 nitrogen atmosphere. From Fig. 8a, the main degradation parameters (Tonset, Tpeak, T10, T20, T50 and W) are 17 extracted and shown in Table 3. Compared with pure polymers, mass losses begin to become significant after 18 250 °C. The variation of the apparent activation energy and pre-exponential factor obtained with Friedman 19 method is presented in Fig. 8b. From this figure, the variation of the activation energy of the thermal 20 degradation versus the conversion function degree deviates from linearity, indicating that the thermal 21 degradation process takes place in more than two stages. Using the MLR method with An and nth equations, 22 the most probable kinetic model for $A-1 \rightarrow B-2 \rightarrow C$ type, coded as d:f; (consecutive reactions) was 23 obtained . The optimal model version for W/DGEBA/EFO/RAMA sample is encoded as d:f; An, Fn, and for 24 W/DGEBA/EHO/RAMA sample encoded as d:f; An, An. The kinetic and statistical parameters obtained for 25 the above models are shown in Table S3 (See Supporting Information). The simulated TG curves obtained 26 based on the data from Table S3, presented in Fig. 8a, are in a good agreement with experimental data, 27 suggesting that the theoretical models accurately approximate the experimental data. For the sample 28 W/DGEBA/EFO/RAMA, in Table S3 in the second degradation step, the reaction order has a value greater 29 than 1, suggesting that oligomers are generated during the thermal degradation process [55].

30

Table 3

1 2

Fig. 8_revised

3

3.6. Chemical composition of the evolved gases

4 In Scheme 3 there is presented the probable mechanism of thermal degradation of the 5 W/DGEBA/EFO/RAMA cured sample. The gaseous products which appear as result of thermal degradation 6 were identified using FT-IR analysis. In Fig. 9a it is shown the 3D FT-IR spectrum and in Fig. 9b the 2D 7 FT-IR spectrum, extracted at the maximum temperature in the Gram Schmidt plot (365 °C) of the evolved 8 gases which appear during thermal degradation of the W/DGEBA/EFO/RAMA cured sample, registered at 9 10 °C min⁻¹. From the 2D FT–IR spectra (Fig. 9b) it is observed a relatively large number of signals located at 3735 cm⁻¹, 3649 cm⁻¹, 3568 cm⁻¹, 3257 cm⁻¹, 2937 cm⁻¹, 2360 cm⁻¹, 1740 cm⁻¹, 1508 cm⁻¹, 1261 cm⁻¹, 1177 10 11 cm⁻¹, 827 cm⁻¹, 669 cm⁻¹ and 538 cm⁻¹. The identification of the signals was made based on literature data 12 [28]. Thus, the signals situated between 3750 and 3500 cm⁻¹ can be attributed to OH groups from water 13 vapors or alcohols which resulted from the thermal degradation of the ester and secondary hydroxyl groups. 14 On the other hand, the signal located at 3257 cm⁻¹ can be assigned to secondary alcohols and phenols which 15 resulted from degradation of lignin and epoxy resin moieties [56]. The signals assigned to CH, CH₂ and CH₃ 16 groups specific to aliphatic and aromatic hydrocarbon residues are located between 3101 cm⁻¹ and 2800 cm⁻¹, 17 as well as 1652 cm⁻¹ and 1461 cm⁻¹ These groups result from oil and DGEBA moieties degradation. The 18 strong signal from 2360 cm⁻¹ can be attributed to carbon dioxide from the degradation of ester groups. 19 Hemicelluloses and cellulose from wood are mainly composed of D-glucopyranose rings, linked together by 20 1–4–glycosidic bonds. By cleaving these linkages, D–glucopyranose rings appear which, by recombination, 21 lead to levoglucosan formation. With temperature rise and in the presence of water levoglucosan is 22 transformed into carboxylic derivatives. The signals between 1860 to 1650 cm⁻¹ with a maximum located at 23 1740 cm⁻¹ can be attributed to acids, ketones, aldehydes and esters moieties, resulted from the degradation of 24 wood, RAMA and oil. The signals between 1650 cm⁻¹ and 1500 cm⁻¹ corroborate with the signal situated at 3014 cm⁻¹ and can be assigned to aromatic rings from benzene, toluene, phenol, α -methyl styrene, 25 26 substances that originate from the degradation of DGEBA, RAMA and lignin moieties. The signals situated at 1261 and 1177 cm⁻¹ can be assigned to ether C–O–C group. 27

- 28
- 29

Scheme 3

- Fig. 9_revised
- 30

1 *3.7. Resistance to fungi*

2	After 10 weeks of exposure to fungi, both the untreated and the polymer treated samples are
3	covered with fungi colonies, more the blank sample and lesser the polymer coated sample (Fig. 10). After
4	washing and conditioning, the untreated wood sample loses up to 19.4 wt. % depending on the type of
5	fungus, while for the polymer coated wood samples, their weight loss is no more than 2 wt. % (Table 4). It
6	can be seen that the strongest attack is due to A. brasiliensis and C. cladosporioides for the untreated samples.
7	The polymer covered samples were more attacked by A. brasiliensis and P. chrysogenum. In the case of
8	pure polymers, all fungi developed very small surface colonies, suggesting that by depositing a thicker layer
9	of polymer may generate an important wood protection effect. Also, in Table 4 there are presented the
10	humidity values after 10 weeks of incubation to fungi exposure. It can be seen that the amount of water
11	absorbed depends on the type of polymer and fungus, the smallest amount being absorbed by
12	W/DGEBA/EHO/RAMA.
13	Fig. 10_revised
14	Table 4
15	
16	3.8. WAXD characterization
17	Figure 11 shows the WAXD curves of the blank and covered samples registered before and after the
18	fungi decay tests. In general, for pure cellulose, four crystalline peaks ($101,10\overline{1}$, 002 and 040) have been
19	identified [57]. In our case, the major diffraction peak specific to the crystalline cellulose is located in the
20	range $22.2 - 22.45^{\circ}$, while the diffraction peak specific for the amorphous phases is situated between 18.6
21	and 18.8° [58, 59]. The fungi preferentially attack the amorphous regions of cellulose, since these regions are
22	less crosslinked in comparison to the crystalline region [60, 61]. These regions may also be highlighted by
23	X-ray analysis. From Table 5 one may observe that the crystallinity index decreases as a result of fungi
24	attack, the lower values being encountered for the unprotected wood samples in comparison with protected
25	samples. This may be due to the blocking by the polymer film of the fungi access to wood.
26	Fig. 11_revised
27	Table 5
28	
29	3.9. SEM and EDAX measurements

1 As an exemplification, the SEM images obtained in radial section with 1 mm thickness for wood 2 and W/DGEBA/EFO/RAMA sample, decayed in the presence of C. cladosporioides, P. chrysogenum and A. 3 brasiliensis are presented in Figure 12. From these images, it can be seen that the raw wood sample masses 4 have developed a large number of fungus hives inside, while the samples protected with 5 DGEBA/EFO/RAMA were not affected. The results are in good agreement with literature data [62]. Using 6 the EDAX analysis it was possible to evaluate the changes in the elemental chemical composition of the 7 surface for raw wood and treated samples after biological decay. Table 6 shows the chemical composition of 8 the sample surfaces for wood and the coated samples. It can be noted that for all the samples there is a 9 significant increase in the percentage of nitrogen as a result of fungal growth. Also, an increase in the 10 percentage of oxygen for the unprotected samples can be observed, which may be due to the appearance of 11 some carboxyl derivatives occurred during cellulose biodegradation. In the case of wood, there appears a 12 significant decrease in the carbon percentage due to the consumption of wood components. The decrease of 13 microelements content may be attributed to the mass increase of the organic product due to the coating 14 process.

Fig. 12

Table 6

- 15
- 16
- 17

18 Conclusions

19 New wood composite materials based on synthetic and natural epoxy derivatives have been 20 obtained and tested in terms of the influence on the thermal stability and fungi resistance. The wood 21 composites were obtained by immersion of the wood samples in a solution of DGEBA/EO/RAMA in 22 acetone and thermally cured. The kinetic parameters of the curing reaction of DGEBA/EO/RAMA and the 23 thermal characterization of crosslinked DGEBA/EO/RAMA and WECs were obtained using DSC and TG 24 methods. The most probable mechanisms of the curing and thermal degradation processes occurred in two or 25 three steps. The decay resistance of wood, DGEBA/EO/RAMA polymers and WECs was obtained by 26 exposure to three fungi (A. brasiliensis, P. chrysogenum and C. cladosporioides) and evaluated with the aid 27 of WAXD and SEM/EDAX methods. Under fungi action, the crystallinity index decreased, the largest drop 28 being registered under the attack of A. brasiliensis. Also, the mass loss was higher after the attack of A. 29 brasiliensis, reaching 19.4 wt. % for wood, while for the WECs this loss was only 2 wt. %. The polymer

1	coatings blocked the access of the fungi in the sample masses, thus inducing a superior resistance to their
2	attack.
3	
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9	SEM/EDAX measuremets.
10	
11	Conflict of interest
12	The authors declare no conflict of interest.
13	
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- 29

30

- 1 Schemes and Figures captions
- 2 **Scheme 1.** The synthesis of epoxy oil.
- **Fig.1.** Variation of the swelling coefficient with the solubility parameter for: (**•**) DGEBA/EFO/RAMA and

4 (O) DGEBA/EHO/RAMA.

- 5 Scheme 2. The possible mechanism of the thermal curing of the DGEBA/EO/RAMA sample.
- 6 **Fig.2.** FT–IR spectra of flax oil (a) and epoxidized flax oil (b).
- 7 **Fig.3.** ¹H–NMR spectra of flax oil (a) and epoxidized flax oil (b).
- 8 Fig.4. FT–IR spectra of W (a), crosslinked DGEBA/EFO/RAMA (b) and WEC (c).
- 9 Fig.5 DSC curves for DGEBA/EFO/RAMA (a) and DGEBA/EHO/RAMA (b) at: (■) 5 °C min⁻¹, at (●) 10
- 10 °C min⁻¹ and at (\blacktriangle) 15 °C min⁻¹ (symbols represent experimental data and lines represent simulated data).
- 11 Fig.6. Dependence of the (\blacksquare) activation energy and the (\bullet) pre–exponential factor versus the conversion
- 12 degree for the curing of: DGEBA/EFO/RAMA (a) and DGEBA/EHO/RAMA (b) calculated with Friedman

13 method.

- 14 **Fig.7.** TG and DTG curves for: DGEBA/EFO/RAMA at: (\blacksquare) 10 °C min⁻¹, at (\bigcirc) 20 °C min⁻¹ and at (\blacktriangle) 30
- 15 °C min⁻¹ (symbols represent experimental data and lines represent simulated data) (a). Dependence of the
- 16 (\blacksquare) activation energy and the (\bullet) pre-exponential factor versus the conversion degree for
- 17 DGEBA/EFO/RAMA calculated with Friedman method (b).
- 18 Fig.8. TG and DTG curves for: DGEBA/EHO/RAMA at: (\blacksquare) 10 °C min⁻¹, at (\bigcirc) 20 °C min⁻¹ and at (\blacktriangle) 30
- ^oC min⁻¹ (symbols represent experimental data and lines represent simulated data) (a). Dependence of the
 (■) activation energy and the (●) pre–exponential factor versus the conversion degree for
 DGEBA/EHO/RAMA calculated with Friedman method (b).
- 22 Scheme 3. The possible mechanism of the thermal degradation of the cured DGEBA/EO/RAMA sample.
- Fig.9. 3D FT-IR and 2D FT-IR spectra, of the evolved gases during thermal degradation of the
 W/DGEBA/EFO/RAMA cured sample, registered at 10 °C min⁻¹ heating rate.
- 25 Fig.10. Blank and the polymer-treated sample exposed to fungi: (a) W, W/DGEBA/EHO/RAMA and 26 DGEBA/EHO/RAMA exposed to A. brasiliensis; (b) W, W/DGEBA/EHO/RAMA and 27 DGEBA/EHO/RAMA exposed to C. cladosporioides; (c) W, W/DGEBA/EHO/RAMA and 28 DGEBA/EHO/RAMA exposed to P. chrysogenum; W/DGEBA/EFO/RAMA (d) W, and
- 29 DGEBA/EFO/RAMA exposed to A. brasiliensis (e) W, W/DGEBA/EFO/RAMA and DGEBA/EFO/RAMA

1	exposed to C. cladosporioides; (f) W, W/DGEBA/EFO/RAMA and DGEBA/EFO/RAMA exposed to P.
2	chrysogenum
3	Fig.11. (a) WAXD curves for: W (1); W decayed with A. brasiliensis (2); W decayed with C.
4	cladosporioides (3); W decayed with P. chrysogenum (4); (b) WAXD curves for: DGEBA/EHO/RAMA
5	decayed with C. cladosporioides (1); DGEBA/EHO/RAMA undecayed (2); DGEBA/EHO/RAMA decayed
6	with A. brasiliensis (3); and DGEBA/EHO/RAMA decayed with P. chrysogenum (4); (c) WAXD curves for:
7	DGEBA/EFO/RAMA decayed with P. chrysogenum (1); DGEBA/EFO/RAMA decayed with C.
8	cladosporioides (2); DGEBA/EFO/RAMA decayed with A. brasiliensis (3) and DGEBA/EFO/RAMA
9	undecayed (4).
10	Fig.12. SEM micrographs of the cross-section of W decayed with: C. cladosporioides (a), P. chrysogenum
11	(b) and A. brasiliensis (c); W/DGEBA/EFO/RAMA decayed with: C. cladosporioides (d), P. chrysogenum
12	(e) and A. brasiliensis (f).
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Number	Solvent	$\delta (\text{cal cm}^{-3})^{0.5}$
1	n-Hexane	7.24
2	Carbon tetrachloride	8.05
3	Cyclohexane	8.18
4	Xilene	8.85
5	Toluene	8.91
6	Ethyl acetate	9.1
7	Chloroform	9.21
8	Tetrahidrofurane	9.52
9	Acetone	9.77
10	Cyclohexanone	9.88
11	Methylene chloride	9.93
12	Dioxane	10
13	Acetic acid	10.1
14	Dimethyl acetamide	11.0
15	Isopropyl alcohol	11.6
16	Dimethyl formamide	12.14
17	Dimethyl sulfoxide	12.93
18	Methanol	14.28
19	Diethylene glycol	14.6
20	Ethylene glycol	16.3
21	Glycerol	21.1
22	Water	23.5

Table 1. Solvents and their corresponding solubility parameters (δ)

Sample	Heating rate	Tonset	T _{peak}	W ₆₀₀	T ₁₀	T ₂₀	T ₅₀
	°C·min ⁻¹	°C	°C	%	°C	°C	°C
	10	380	422	1.2	259	374	413
DGEBA/EFO/RAMA	20	380	427	2.1	325	374	418
	30	378	430	5.2	331	375	425
DGEB 4/EHO/R 4 M 4	10	383	419	1.1	339	380	419
DOLDAYENO/MANAY	20	383	429	2.2	355	387	429
	30	377	436	5.4	363	390	499

Table 2.

Thermal degradation parameters obtained by TG analysis of cured samples at three heating rates.

T_{onset} – the temperature at which the thermal degradation start;

 T_{peak} – the temperature at which the degradation rate is maximum;

 T_{10} , T_{20} , T_{50} - the temperatures corresponding to 10 wt.%, 20 wt.%, 50 wt.% mass losses; W_{600} - residual mass at 600 °C

Table 3.

The thermal parameters obtained by TG analysis of cured W/DGEBA/EO/RAMA samples at three heating rates

Sample	Heating rate	Tonset	T _{peak}	W ₆₀₀	T ₁₀	T ₂₀	T ₅₀
	°C·min ⁻¹	°C	°C	%	°C	°C	°C
	10	319	356	17.4	286	320	361
W/DGEBA/EFO/RAMA	20	322	363	27.8	286	326	370
	30	323	365	20.9	285	328	378
W/DGEBA/EHO/RAMA	10	321	354	20.5	296	323	362
	20	329	364	22.9	302	330	380
	30	320	371	20.2	298	330	381

T_{onset} – the temperature at which the thermal degradation starts;

 T_{peak} – the temperature at which the degradation rate is maximum;

 T_{10} , T_{20} , T_{50} - the temperatures corresponding to 10 wt.%, 20 wt.%, 50 wt.% mass losses;

 $W_{600}\text{-}$ residual mass at 600 ^{o}C

Table 4. Some characteristic of the samples, registered after a10 week exposure against *A. brasiliensis*, *P. chrysogenum* and *C. cladosporioides* strains.

Sample		mean weight loss ^a		humidity ^{a,}				
		WL (%)		Н (%)				
	A. brasiliensis	P. chrysogenum	C. cladosporioides	A. brasiliensis	P. chrysogenum	C. cladosporioides		
W	19.4	4.47	6.37	50.4	50.5	33.5		
W/DGEBA/EHO/RAMA	1.82	1.38	0.43	6.97	22.6	26.7		
W/DGEBA/EFO/RAMA	1.89	1.39	1.22	38.5	36.9	16.7		

a) Means were for 4 samples

Table 5. Crystalline index

Sample	Undecayed blank	A. brasiliensis	P. chrysogenum	C. cladosporioides
		decayed	decayed	decayed
W	74.0	67.58	70.04	70.1
W/DGEBA/EHO/RAMA	67.4	63.2	64.4	64.13
W/DGEBA/EFO/RAMA	69.2	63.6	67.7	67.0

Means were for 4 samples

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Table 6. SEM/EDAX composition of wood and W/DGEBA/EO/RAMA samples

	Sample									
Element	t W			W/DGEBA/EHO/RAMA			W/DGEBA/EFO/RAMA			
	undecayed	decayed with	decayed with	decayed with	decayed with	decayed with	decayed with	decayed with	decayed with	decayed with
		C. cladosporioides	P.chrysogenum	A.brasiliensis	C. cladosporioides	P.chrysogenum	A.brasiliensis	C. cladosporioides	P.chrysogenum	A.brasiliensis
С	66.2	58.42	58.45	55.85	71.68	70.52	71.94	68.65	58.30	69.08
Ν	1.66	4.60	3.55	4.51	4.62	6.10	5.45	3.77	5.31	4.72
0	30.11	35.23	36.82	36.4	23.63	25.2	21.20	33.22	35.15	32.63
Fe	0.62	0.63	0.30	0.61	0.33	0.39	0.25	0.47	0.23	0.63
Na	0.24	0.23	0.24	0.45	0.10	0.15	0.11	0.16	0.13	0.11
Mg	0.04	0.04	0.05	0.07	0.09	0.06	0.20	0.08	0.10	0.08
Al	0.18	0.11	0.06	0.06	0.08	0.12	0.29	0.11	0.12	0.12
Si	0.25	0.14	0.16	0.21	0.12	0.10	0.11	0.10	0.13	0.11
Cl	0.17	0.15	0.14	0.02	0.18	0.15	0.12	0.09	0.12	0.19
K	0.16	0.20	0.17	0.15	0.17	0.08	0.89	0.07	0.14	0.13
Ca	0.16	0.16	0.13	0.14	0.11	0. 10	0.19	0.15	0.12	0.11
				4						











Series











d W, W/DGEBA/EFO/RAMA, DGEBA/EFO/RAMA exposed to A. brasiliensis





W decayed with Cladosporium cladosporioides (a)



 $\ensuremath{\mathrm{W/DGEBA/EFO/RAMA}}$ decayed with Cladosporioum cladosporioides (d)



W decayed with Penicilium chrysogenum (b)



W/DGEBA/EFO/RAMA decayed with Penicilium chrysogenum (e)



W decayed with Aspergillus brasiliensis (c)



W/DGEBA/EFO/RAMA decayed with A spergillus brasiliensis (f)



 $CH_3COOH + H_2O_2 \xrightarrow{H^+} CH_3COOOH + H_2O$ peracetic acid acetic acid $CH = OC - (CH_{27} - CH = CH - CH_2 - CH = CH - CH_2 - CH = CH - CH_2 - CH_3$ $\begin{array}{c} \begin{array}{c} 2 \\ CH-OC-(CH_2)_7-CH=CH-CH_2-CH=CH-(CH_2)_4-CH_3 \\ \end{array} + CH_3COOOH \xrightarrow{H^+} \begin{array}{c} 0 \\ CH-OC-(CH_2)_7-CH-CH-CH_2-CH-CH_2-CH-(CH_2)_4-CH_3 \\ \end{array} \\ \end{array}$ + CH₃COOH $\begin{array}{c} \mathsf{C} \mathsf{H}_{-\mathsf{O}}\mathsf{C} \mathsf{C} \mathsf{-} (\mathsf{C} \mathsf{H}_2)_{7} - \underbrace{\mathsf{C} \mathsf{H}_{-} \mathsf{C} \mathsf{H}_{2} - \underbrace{\mathsf{C} \mathsf{H}_{-} \mathsf{C} \mathsf{H}_{-} \mathsf{C} \mathsf{H}_{2} - \underbrace{\mathsf{C} \mathsf{H}_{-} \mathsf{C} \mathsf{H}_{2} - \underbrace{\mathsf{C} \mathsf{H}_{-} \mathsf{C} \mathsf{H}_{2} - \underbrace{\mathsf{C} + \underbrace{\mathsf{C$ $O_{CH_{7}OC} - (CH_{2})_{7} - CH = CH - CH_{2} - CH = CH - CH_{2} - CH = CH - CH_{2} - CH_{3}$ FO EFO Scheme 2



- New synthetic and natural epoxy derivatives as wood coatings were obtained.
- The epoxy derivatives were thermally crosslinked.
- The influence of coating on wood thermal stability and fungi resistance was made.