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- **Thermal behaviour and fungi resistance of composites based on wood and natural and synthetic epoxy resins cured with maleopimaric acid**
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Abstract

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Poni" Institute of Macromolecular Chemistry, 41A Gr. Ghica Wood/epoxy resin composites based on diglycidyl ether of bisphenol A (DGEBA)/epoxidized oil (EO)/Diels–Alder adducts of resin acids with maleic anhydride (RAMA) in acetone (80 %) were obtained by 12 impregnation. Epoxidation was carried out in the presence of hydrogen peroxide (H_2O_2) , acetic acid (AAc), sulfuric acid (H2SO4) as catalyst and cyclohexane (CHx) as solvent at a molar ratio of 0.5/1.5/1 (AAc/hydrogen peroxide/ethylene unsaturation). The kinetic parameters (activation energy and pre– exponential factor) of the DGEBA/EO/RAMA curing reaction and thermal characterization of the crosslinked compounds and wood epoxy composites (WECs) were obtained using differential scanning calorimetry (DSC) and thermogravimetric analysis (TGA). Based on the chemical structure of the evolved gases resulted during thermal decomposition of the crosslinked polymers and WECs, identified with FT–IR, a probable mechanism of thermal degradation was proposed. Resistance to three fungi was also tested. **Keywords:** Wood, Thermosetting resin, Cure behaviour, Thermal properties, Biological resistance

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1. Introduction

Nowadays, composites based on natural materials are widely used in industrial and household fields, because they are environmentally friendly and originate from renewable resources. Wood is among the most important renewable resources. It has a great importance for life sustainability, as well as both raw and processed material. The most important components of wood are lignin, cellulose, hemicelluloses and resins. Under environmental factors influence (i.e. temperature, light, moisture, microorganisms, insects, etc.), there occurs wood damage, followed by a decrease in technical (thermal, mechanical and electrical behaviour) and aesthetic aspects [1, 2].

To preserve the properties of wood, physical and chemical methods, including heat treatment, chemical modification, impregnation and physical coatings, have been used. Considering its chemical structure (mainly hydroxyl groups), wood was modified by esterification and etherification reactions with anhydrides, acids, acid chlorides, epoxy resins, unsaturated derivatives, cyclic ethers, lactones, alkyl chlorides and so on. These transformations were aimed to improve mechanical and electrical properties, as well as to enhance resistance to environmental factors action [3–13].

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and damage, followed by a decrease in ucchnical (thermal, mechanical and electrical behavious

apspects [1, 2].

To preserve t Vegetable oils (edible or non–edible) are a renewable source of raw materials, mainly esters of glycerol, which are the result of glycerol esterification with three saturated and/or unsaturated fatty acids [14]. As a consequence of the chemical structures, these oils may be modified to obtain new monomers that can induce special properties in the final polymers (flexibility, biocompatibility, biodegradability, thermal stability) [4, 15–20]. Hemp oil and flax oil, as non–edible oils that contain a large number of unsaturated groups in their structure, represent an excellent source of raw material for the synthesis of monomers with new functional groups capable to polymerize. One of the most common methods of chemical modification of vegetable oils is epoxidation. Epoxidized oils may be used as basis for their transformation in acrylated, methacrylated, hydroxylated monomers, used either individually or mixed in various polymeric compositions [16, 17, 21–25]. Also, vegetable oils and their derivatives, alone or in combination with various fungicides, have been used to increase the decay resistance of wood [26, 27].

Rosin is a renewable naturally raw material consisting of neutral compounds (turpentine) and resin acids (abietic, levopimaric, neoabietic, palustric, fatty acids, etc.). As a consequence of their chemical structure, the resin acids can be converted into several types of monomers. In particular, the most common transformation is the Diels–Alder reaction, when some polyacids are obtained and further used as

crosslinking agents for epoxy resins [28–35]. These adducts, through their chemical structure, may improve the properties of the crosslinked epoxy resins.

Epoxy resins are some of the most widely available synthetic monomers, which, after curing, present excellent electrical, mechanical and thermal properties in a vast palette of application fields, although not being environmentally friendly [36, 37]. This behaviour depends on the formulation, chemical composition and crosslinking conditions. By using some natural ingredients (rosin acids and vegetable oil derivatives), these formulations may compensate some drawbacks and be environmentally friendly [16, 20, 28–35, 38, 39].

The paper describes the curing and non–isothermal degradation kinetics of compositions based on DGEBA/EO/RAMA and WECs. The novelty of the work consists in the using of some epoxy resins based on vegetable oils and of a curing agent derived from resinic acids of natural origin. Also, the thermal and fungal resistance properties were followed using DSC and TG analyses. Based on FT–IR analysis of the evolved gases during thermal decomposition a possible degradation mechanism is proposed.

2. Experimental

2.1. Materials

ion and crosslinking conditions. By using some natural ingredients (rosin acids and vegetats), these formulations may compensate some drawbacks and be environmentally friendly [1]

S, 39].

The paper describes the curing 17 Hydrogen peroxide $(H₂O₂)$, glacial acetic acid (AAc), maleic anhydride (MA), potassium hydroxide (KOH), sulfuric acid (H2SO4)*,* triethylbenzylammonium chloride (TEBAC) and anhydrous sodium sulfate (Na₂SO₄) were analytical grade products and used without any purification. The solvents were used as received or distilled before use. Resin acids (RA) were obtained from commercial rosin by acid isomerization and by repeated recrystallizations from concentrated acetone solutions and had an acid number 22 (a. n.) of 181 mg KOH g^{-1} and melting point (m. p.) of 161 °C [33]. RAMA with m. p. 230 °C and a. n. 434 23 mg KOH g^{-1} was obtained following a procedure described in the literature [40]. DGEBA, a commercial 24 product (Sintofarm, Romania), (average epoxy equivalent weight of 190 g eq⁻¹, viscosity of 12000 mPas at 25 25 °C) was used as received. Flax oil (FO) and hemp oil (HO) have been obtained from the local market and have the following compositions supplied by the manufacturers: flax oil [saturated fats 10.1 wt. %, unsaturated fats (oleic acid 22.4 wt. %, linoleic acid 14.3 wt. %, α–linolenic acid 52.3 wt. %), other acids 0.9 wt. %] and hemp oil [saturated fats 8 wt. %, unsaturated fats (oleic acid 11.4 wt. %, linoleic acid 57 wt. %, 29 α –linolenic acid 18.7 wt. %, other acids 2.9 wt. %)]. Epoxidized flax oil (EFO) (number of epoxy groups 5.9 30 mol^{-1}) was obtained as described below and epoxidized hemp oil (EHO) (number of epoxy group 3.5 mol⁻¹)

1 was obtained following a procedure described in the literature [23]. The number of epoxy groups was 2 measured using ¹H–NMR spectroscopy. The softwood samples (W) (*Abies alba L*.) had the same 3 characteristics as those presented in a previous work [9].

4

5 *2.2. Sample preparation for DSC and TGA studies*

For the DSC studies, the formulation DGEBA/EO/RAMA at a molar ratio of 0.8/0.2/0.66 (epoxy ring/carboxyl proton 1/1) in the presence of TEBAC as catalyst was prepared. After a vigorous mixing of the 8 reactants, they were degassed in a vacuum oven at room temperature and a portion has been stored at 0 °C before the DSC recording was performed. The DGEBA/EO/RAMA compositions used for the TG characterization were transferred in an aluminum form and crosslinked according to the following protocol: 1 11 h at 100 °C, 1 h at 135 °C and post cured 4 h at 185 °C (Scheme 1).

12 **Scheme 1**

For the DSC studies, the formulation DGEBA/EO/RAMA at a molar ratio of 0.80,20.66 (bysyl protion 1/1) in the presence of TEBAC as catalyst was prepared. After a vigorous mixing they were degassed in a vacuum oven at room 13 The WEC samples were obtained by immersion of W samples for 8 h in the next formulation: 14 DGEBA/EO/RAMA at molar ratio 0.8/0.2/0.66, 80 wt. % solution in acetone, in the presence of TEBAC as 15 catalyst. After immersion, the impregnated samples were placed in a vacuum oven at 40 °C and maintained 16 another 8 h to release the solvent. Then, the WECs were cured at 70 °C for 1 h, 1 h at 100 °C, 1 h at 135 °C 17 and then post cured at 150 °C for 3 h and used for TGA studies. The same samples were also used for 18 crystallinity measurements and for morphological analysis. The weight fraction of W in WECs was 90 %.

19

20 *2.3. Measurements and methods*

21 The acid number (a.n.) was obtained using a slightly modified ASTM D 465–05. The sample 22 dissolved in acetone at 10 % (w/v) concentration was titrated with 0.5 N ethanolic KOH solutions in the 23 presence of phenolphthalein as indicator [35, 41]. The epoxy equivalent weights (EEW) were obtained using 24 ASTM D 1652-04 [42]. The number of the double bonds from oils was obtained using $H-MMR$ 25 spectroscopy, with the next equation [43]:

$$
D_b = 0.5(A - N_f) / N_f \tag{1}
$$

27 where: D_b is the double bonds number, A is the surface 28 assigned to the olefinic protons located between 5.2 and 5.4 ppm and N_f is the normalization factor (obtained 29 through the dividing by 4 of the protons area from 4.0 and 4.3 ppm assigned to terminal protons of glycerol).

1 The melting points were obtained with a DSC 200 F3 Maia device (Netzsch, Germany), at 10 °C min⁻¹ 2 heating rate.

3 FT-IR spectra were acquired with a Vertex 70 apparatus (Bruker–Germany) using KBr pellets. ¹H–NMR 4 spectra of DGEBA, oils, epoxidized oils and RAMA were recorded with an Avance DRX 400 (Bruker– 5 Germany) apparatus at 50 °C using CDCl₃ and DMSO– d_6 as solvents and tetramethylsilane (TMS) as 6 internal standard.

andard.

So were recorded in the temperature range 30–600 °C, in inert atmosphere (N₂ flow rate of chree heating rates (10, 20 and 30 °C min⁺¹) using STA 449 F1 Jupiter device (Negzsch-Gern

O, erneibles were loaded w TG curves were recorded in the temperature range 30–600 °C, in inert atmosphere (N_2 flow rate of 40 mL δ min⁻¹) at three heating rates (10, 20 and 30 °C min⁻¹) using STA 449 F1 Jupiter device (Netzsch–Germany). 9 Open Al_2O_3 crucibles were loaded with approximately 10 mg of the ground sample. Gaseous products 10 resulting from thermal degradation were transferred through a transferring line made from Teflon, coupled to 11 the head of the TG balance, with 1 m length and with 1.5 mm diameter (heated at 190 °C to limit 12 condensation) to the FTIR apparatus having a MCT detector (Mercury Cadmium Telluride). The FT–IR 13 spectra were recorded between 4000 and 500 cm⁻¹ wavenumber values and processed with OPUS 6.5 14 software.

DSC analysis was undertaken on a DSC 200 F3 Maia apparatus (Netzsch, Germany), under nitrogen flow 16 rate of 50 mL min⁻¹, at three heating rates (5, 10 and 15 $^{\circ}$ C min⁻¹) in the temperature range 25–300 $^{\circ}$ C. The calibration of the apparatus was made with high purity indium. The samples weighing up to 10 mg were placed in aluminum cells provided with a pierced lid, were scanned in the presence of one aluminum empty cell as standard. The heat flow versus temperature was recorded. DSC data were recorded consecutively using the same sample on the same day [44].

The evaluation of the kinetic parameters, both for curing and thermal degradation reactions were obtained using DSC and TG scans and processed with Netzsch Thermokinetics 3 software [45]. In a first instance, these parameters were evaluated on the basis of free–estimation methods of Ozawa–Flynn–Wall (OFW) and Friedman (FD). The used equations are as follows [46–48].

$$
\ln \beta = C - 1.052(E_0/RT_p) \tag{2}
$$

26 and

27
$$
\ln\left(\frac{d\alpha}{dT}\right) = \ln\left(\frac{A}{\beta}\right) + \ln(f(\alpha)) - \frac{E_{FD}}{RT}
$$
 (FD equation) (3)

1 where: *A* is the frequency factor, β is the heating rate, *C* is a constant, E_0 and E_{FD} are the specific activation 2 energies of reactions obtained with OFW and FD relations, T_p is the exothermic peak temperature in Kelvin and *R* is universal gas constant.

These methods, included in "Netzsch Thermokinetics 3", a software module for the kinetic analysis of thermal measurements, permit the evaluation of the kinetic parameters and the variation of activation energy values versus conversion degree, without assuming any reaction model. Changes in the shape of the activation energy versus the degree of conversion curves indicate that the degradation reactions occur following a complex mechanism in several independent stages through consecutive, parallel or competitive processes [49, 50]. This makes it possible to choose between different mechanisms and obtain a global model that gives the best results for the curing or thermal degradation processes.

Morphological study of WECs was conducted by analyzing the scanning electron microscopy (SEM) images. These were obtained using the SEM/ESEM–EDAX–QUANTA 200 apparatus which operated in the following parameters: field emission filament 16 kV accelerating voltage, high vacum mode and maximum magnification of 5000 X. The images were obtained on the surface samples, cut perpendicularly on the sense of growth and gilded to make them conductive.

ersus conversion degree, without assuming any reaction model. Changes in the shape
of energy versus the degree of conversion curves indicate that the degradation reactions
a complex mechanism in several independent stages Anti–decay resistance testing was performed on untreated wood (blank), polymer and WECs. The test samples were obtained as previously described above. The main components of wood (cellulose, hemicelluloses, lignin), under favorable conditions of humidity and temperature, can be metabolized by fungi as nutrients, resulting in wood degradation. Four samples from each specimen, dried to constant weight at 20 105 °C, were tested in the same conditions for resistance against decay. The following fungi were used: a white rot fungus *Penicillium chrysogenum* ATCC10106 (*P. chrysogenum*), a brown rot fungus *Cladosporium cladosporioides* ATCC16022 (*C. cladosporioides*) and black rot fungus *Aspergillus brasiliensis* ATCC 9642 (*A. brasiliensis*). The samples were placed in Petri dishes on a substrate of malt extract (for *P. chrysogenum*) and potato dextrose (for *C. cladosporioides* and *A. brasiliensis*) in agar which were previously inoculated 25 with a standard inoculum of 0.5 McFerland for each fungal strain. All the Petri dishes were incubated at the 26 room temperature (24 \pm 1 °C) for 10 weeks. The fungal growth on the untreated and treated samples was monitored during the 10 weeks of incubation and at the end of the experiment the wood samples were removed from the culture plates and the fungal biomass was gently removed with the aid of a wet cotton 29 fabric. The wet samples were oven–dried at 105 $^{\circ}$ C, in order to reach constant weight. Then all the samples were accurately weighed in order to notice the retained moisture.

The solubility parameter of the crosslinked samples is obtained by observing the maximum of the swelling 2 coefficient (Q) in the Q versus δ plot (Fig.1). As it may be seen from Fig. 1, the maximum value is reached for methylene chloride, which is the solvent that induces the highest degree of network swelling. It can be 4 considered that the solubility parameter of methylene chloride, of 9.93 (cal cm⁻³)^{0.5}, may be attributed to the polymer–solvent interaction parameter of the crosslinked polymers. The molecular weight between two crosslinking points (Mc) and the crosslinking density (n) of DGEBA/EO/RAMA samples were obtained based on the swelling measurements and calculated with Flory–Rehner equation [54]:

8
$$
n = -[\ln(1-V) + V + \chi \bullet V^2]/V_{mol}[V^{0.33} - V/2]
$$
 (9)

9 where: *V* is the volume fraction of polymer in swollen polymer, V_{mol} is the molar volume of the solvent and 10γ is the Flory solvent–polymer interaction parameter. The interaction parameter may be obtained with the 11 equation:

12
$$
\chi = \frac{V}{RT} (\delta_p - \delta_s)^2
$$
 (10)

13 where: *R* is the gas constant, *T* is temperature in Kelvin, *V* is the molar volume of the solvent, δ_p is 14 solubility parameter of polymer and δ_s is solubility parameter of solvent.

15

16 **3. Results and discussion**

17 *3.1. Synthesis and characterization of epoxidized flax oil (EFO)*

mg points (Mc) and the crosslinking density (n) of DGEBA/EO/RAMA samples were obthe swelling measurements and calculated with Flory–Rehner equation [54]:
 $n = -\ln(1-V) + V + \chi \cdot V^2]/V_{\text{med}}[V^{0.33} - V/2]$

is the volume fraction 18 Into a 0.5 L four–necked reaction vessel placed in a water bath, equipped with mechanical stirrer, 19 thermometer, a water reflux condenser and dropping funnel, 150 g FO, 120 g AAc, 2 mL H₂SO₄ (diluted in 4 20 mL of distilled water) and 40 mL CHx were introduced. CHx was used to reduce the viscosity of the mixture 21 and to minimize the epoxy cycle opening. The reaction mixture was moderately stirred for about 30 minutes, 22 purged with a slow flow of nitrogen and the water bath was cooled with ice to 10 °C. After 1 h, 220 g H₂O₂ 23 30 % (w/w) was added in small portions under vigorous stirring, while maintaining the reaction mixture 24 temperature at about 15 °C. After adding the entire amount of H_2O_2 , the temperature of the reaction mixture 25 was slowly raised to 55 °C and maintained at this level for another 6 h. For finishing the reaction, the 26 mixture was heated to 65 °C for another 0.5 h and then cooled rapidly on ice water bath. The reaction mass 27 was washed twice with distilled water at 35 \degree C and then with a 5 wt. % potassium carbonate solution until 28 complete neutralization. Then, the water layer was discharged and EFO was kept on anhydrous sodium

30 cm^{-1} and 1028 cm⁻¹ (C–O–C stretching vibrations) (Figs 4b and 4c). There may also be observed a series of

27 at high speeds, present only an exothermic peak, suggesting that all chemical reactions occur simultaneously.

28 The evaluation of the kinetic parameters of the crosslinking reactions (apparent activation energy and

29 preexponential factor) of the above samples was undertaken using the Friedman (FD) and Ozawa (OZ)

30 methods [45–48].

10

-
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Fig. 7_revised

Table 2

Using the data from Table S2 the TG curves were recalculated. Good overlapping of experimental and calculated data curves may be observed (Fig. 7a).

(See Supporting Information). The activation energies for the first stage of degradation depeats structure of epoxy oil and have a value of 302 M mol⁻¹ for DGEBA/EFO/RAMA sample :

Dr¹² for DGEBA/EHO/RAMA sample, whil In the case of WECs, the thermal characterization was obtained with same software. Fig. 8a presents the TG and DTA curves of W/DGEBA/EHO/RAMA sample obtained at three heating rates in 16 nitrogen atmosphere. From Fig. 8a, the main degradation parameters $(T_{onset}, T_{peak}, T_{10}, T_{20}, T_{50}$ and *W*) are extracted and shown in Table 3. Compared with pure polymers, mass losses begin to become significant after 18 250 °C. The variation of the apparent activation energy and pre-exponential factor obtained with Friedman method is presented in Fig. 8b. From this figure, the variation of the activation energy of the thermal degradation versus the conversion function degree deviates from linearity, indicating that the thermal 21 degradation process takes place in more than two stages. Using the MLR method with An and nth equations, 22 the most probable kinetic model for A-1 \rightarrow B-2 \rightarrow C type, coded as d:f; (consecutive reactions) was 23 obtained . The optimal model version for W/DGEBA/EFO/RAMA sample is encoded as d:f; An, Fn, and for W/DGEBA/EHO/RAMA sample encoded as d:f; An, An. The kinetic and statistical parameters obtained for the above models are shown in Table S3 (See Supporting Information). The simulated TG curves obtained based on the data from Table S3, presented in Fig. 8a, are in a good agreement with experimental data, suggesting that the theoretical models accurately approximate the experimental data. For the sample W/DGEBA/EFO/RAMA, in Table S3 in the second degradation step, the reaction order has a value greater than 1, suggesting that oligomers are generated during the thermal degradation process [55].

Table 3

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2

1 **Fig. 8_revised**

3 *3.6. Chemical composition of the evolved gases*

utified using FT-IR analysis. In Fig. 9a it is shown the 3D FT-IR spectrum and in Fig. 9b
tectrum, extracted at the maximum temperature in the Gram Schmidt plot (365 °C) of the ex
for the appear during thermal degradation 4 In Scheme 3 there is presented the probable mechanism of thermal degradation of the 5 W/DGEBA/EFO/RAMA cured sample. The gaseous products which appear as result of thermal degradation 6 were identified using FT–IR analysis. In Fig. 9a it is shown the 3D FT–IR spectrum and in Fig. 9b the 2D 7 FT–IR spectrum, extracted at the maximum temperature in the Gram Schmidt plot (365 $^{\circ}$ C) of the evolved 8 gases which appear during thermal degradation of the W/DGEBA/EFO/RAMA cured sample, registered at 9 . 10 $^{\circ}$ C min⁻¹. From the 2D FT–IR spectra (Fig. 9b) it is observed a relatively large number of signals located 10 at 3735 cm⁻¹, 3649 cm⁻¹, 3568 cm⁻¹, 3257 cm⁻¹, 2937 cm⁻¹, 2360 cm⁻¹, 1740 cm⁻¹, 1508 cm⁻¹, 1261 cm⁻¹, 1177 11 cm⁻¹, 827 cm⁻¹, 669 cm⁻¹ and 538 cm⁻¹. The identification of the signals was made based on literature data $[28]$. Thus, the signals situated between 3750 and 3500 cm⁻¹ can be attributed to OH groups from water 13 vapors or alcohols which resulted from the thermal degradation of the ester and secondary hydroxyl groups. 14 On the other hand, the signal located at 3257 cm^{-1} can be assigned to secondary alcohols and phenols which 15 resulted from degradation of lignin and epoxy resin moieties [56]. The signals assigned to CH, CH₂ and CH₃ 16 groups specific to aliphatic and aromatic hydrocarbon residues are located between 3101 cm⁻¹ and 2800 cm⁻¹, 17 as well as 1652 cm⁻¹ and 1461 cm⁻¹ These groups result from oil and DGEBA moieties degradation. The 18 strong signal from 2360 cm^{-1} can be attributed to carbon dioxide from the degradation of ester groups. 19 Hemicelluloses and cellulose from wood are mainly composed of D–glucopyranose rings, linked together by 20 1–4–glycosidic bonds. By cleaving these linkages, D–glucopyranose rings appear which, by recombination, 21 lead to levoglucosan formation. With temperature rise and in the presence of water levoglucosan is 22 transformed into carboxylic derivatives. The signals between 1860 to 1650 cm⁻¹ with a maximum located at 23 1740 cm⁻¹ can be attributed to acids, ketones, aldehydes and esters moieties, resulted from the degradation of 24 wood, RAMA and oil. The signals between 1650 cm⁻¹ and 1500 cm⁻¹ corroborate with the signal situated at 25 and 25 and can be assigned to aromatic rings from benzene, toluene, phenol, α –methyl styrene, 26 substances that originate from the degradation of DGEBA, RAMA and lignin moieties. The signals situated 27 at 1261 and 1177 cm^{-1} can be assigned to ether C–O–C group.

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-

28 **Scheme 3**

- 29 **Fig. 9_revised**
- 30

3.7. Resistance to fungi

X analysis it was possible to evaluate the changes in the elemental chemical composition
or raw wood and treated samples after biological decay. Table 6 shows the chemical composition
to trace state of the coated samples. As an exemplification, the SEM images obtained in radial section with 1 mm thickness for wood and W/DGEBA/EFO/RAMA sample, decayed in the presence of *C. cladosporioides, P. chrysogenum* and *A. brasiliensis* are presented in Figure 12. From these images, it can be seen that the raw wood sample masses have developed a large number of fungus hives inside, while the samples protected with DGEBA/EFO/RAMA were not affected. The results are in good agreement with literature data [62]. Using the EDAX analysis it was possible to evaluate the changes in the elemental chemical composition of the surface for raw wood and treated samples after biological decay. Table 6 shows the chemical composition of the sample surfaces for wood and the coated samples. It can be noted that for all the samples there is a significant increase in the percentage of nitrogen as a result of fungal growth. Also, an increase in the percentage of oxygen for the unprotected samples can be observed, which may be due to the appearance of some carboxyl derivatives occurred during cellulose biodegradation. In the case of wood, there appears a significant decrease in the carbon percentage due to the consumption of wood components. The decrease of microelements content may be attributed to the mass increase of the organic product due to the coating process.

- **Fig. 12**
- **Table 6**
-

Conclusions

New wood composite materials based on synthetic and natural epoxy derivatives have been obtained and tested in terms of the influence on the thermal stability and fungi resistance. The wood composites were obtained by immersion of the wood samples in a solution of DGEBA/EO/RAMA in 22 acetone and thermally cured. The kinetic parameters of the curing reaction of DGEBA/EO/RAMA and the thermal characterization of crosslinked DGEBA/EO/RAMA and WECs were obtained using DSC and TG methods. The most probable mechanisms of the curing and thermal degradation processes occurred in two or three steps. The decay resistance of wood, DGEBA/EO/RAMA polymers and WECs was obtained by exposure to three fungi (*A. brasiliensis, P. chrysogenum* and *C. cladosporioides*) and evaluated with the aid of WAXD and SEM/EDAX methods. Under fungi action, the crystallinity index decreased, the largest drop being registered under the attack of *A. brasiliensis*. Also, the mass loss was higher after the attack of *A. brasiliensis*, reaching 19.4 wt. % for wood, while for the WECs this loss was only 2 wt. %. The polymer

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- 1 **Schemes and Figures captions**
- 2 **Scheme 1.** The synthesis of epoxy oil.
- 3 Fig.1. Variation of the swelling coefficient with the solubility parameter for: (\bullet) DGEBA/EFO/RAMA and

4 (O) DGEBA/EHO/RAMA.

- 5 **Scheme 2.** The possible mechanism of the thermal curing of the DGEBA/EO/RAMA sample.
- 6 **Fig.2.** FT–IR spectra of flax oil (a) and epoxidized flax oil (b).
- **Fig.3.** ¹H–NMR spectra of flax oil (a) and epoxidized flax oil (b).
- 8 **Fig.4.** FT–IR spectra of W (a), crosslinked DGEBA/EFO/RAMA (b) and WEC (c).
- **Fig.5** DSC curves for DGEBA/EFO/RAMA (a) and DGEBA/EHO/RAMA (b) at: (\blacksquare) 5 °C min⁻¹, at (\lozenge) 10
- 10 $^{\circ}$ C min⁻¹ and at (\triangle) 15 $^{\circ}$ C min⁻¹ (symbols represent experimental data and lines represent simulated data).
- 11 **Fig.6.** Dependence of the (■) activation energy and the (●) pre–exponential factor versus the conversion
- 12 degree for the curing of: DGEBA/EFO/RAMA (a) and DGEBA/EHO/RAMA (b) calculated with Friedman
- 13 method.
- **Fig.7.** TG and DTG curves for: DGEBA/EFO/RAMA at: (\blacksquare) 10 °C min⁻¹, at (\lozenge) 20 °C min⁻¹ and at (\blacktriangle) 30
- 15 °C min⁻¹ (symbols represent experimental data and lines represent simulated data) (a). Dependence of the
- 16 (a) activation energy and the (\bullet) pre–exponential factor versus the conversion degree for
- 17 DGEBA/EFO/RAMA calculated with Friedman method (b).
- **Fig.8.** TG and DTG curves for: DGEBA/EHO/RAMA at: (1) 10 °C min⁻¹, at (\bullet) 20 °C min⁻¹ and at (\blacktriangle) 30
- -IR spectra of flax oil (a) and epoxidized flax oil (b).

-NMR spectra of lax oil (a) and epoxidized flax oil (b).

-NMR spectra of W (a), crosslinked DGEBA/EFO/RAMA (b) and WEC (c).

C curves for DGEBA/EFO/RAMA (a) and D 19 °C min⁻¹ (symbols represent experimental data and lines represent simulated data) (a). Dependence of the 20 $($ $)$ activation energy and the $($ ^{$)$} pre–exponential factor versus the conversion degree for 21 DGEBA/EHO/RAMA calculated with Friedman method (b).
- 22 **Scheme 3.** The possible mechanism of the thermal degradation of the cured DGEBA/EO/RAMA sample.
- 23 **Fig.9.** 3D FT–IR and 2D FT–IR spectra, of the evolved gases during thermal degradation of the 24 W/DGEBA/EFO/RAMA cured sample, registered at 10° C min⁻¹ heating rate.
- 25 **Fig.10.** Blank and the polymer-treated sample exposed to fungi: (a) W, W/DGEBA/EHO/RAMA and 26 DGEBA/EHO/RAMA exposed to *A. brasiliensis;* (b) W, W/DGEBA/EHO/RAMA and 27 DGEBA/EHO/RAMA exposed to *C. cladosporioides*; (c) W, W/DGEBA/EHO/RAMA and 28 DGEBA/EHO/RAMA exposed to *P. chrysogenum*; (d) W, W/DGEBA/EFO/RAMA and 29 DGEBA/EFO/RAMA exposed to *A. brasiliensis* (e) W, W/DGEBA/EFO/RAMA and DGEBA/EFO/RAMA

Table 1. Solvents and their corresponding solubility parameters (δ)

Table 2**.**

Thermal degradation parameters obtained by TG analysis of cured samples at three heating rates.

Tonset – the temperature at which the thermal degradation start;

Tpeak – the temperature at which the degradation rate is maximum;

 T_{10} , T_{20} , T_{50} - the temperatures corresponding to 10 wt.%, 20 wt.%, 50 wt.% mass losses;

 W_{600} - residual mass at 600 °C

Table 3.

The thermal parameters obtained by TG analysis of cured W/DGEBA/EO/RAMA samples at three heating rates

Tonset – the temperature at which the thermal degradation starts;

 T_{peak} – the temperature at which the degradation rate is maximum;

 T_{10} , T_{20} , T_{50} - the temperatures corresponding to 10 wt.%, 20 wt.%, 50 wt.% mass losses;

 W_{600} - residual mass at 600 °C

Table 4. Some characteristic of the samples, registered after a10 week exposure against *A. brasiliensis*, *P. chrysogenum* and *C. cladosporioides*strains.

a) Means were for 4 samples

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accept after all 0 week exposure against A. brasiliensis,

mean weight loss⁸

WL (%)

is P. chrysogenum C. cladosporioides A. brasiliensis

4.47 6.37 50.4

1.38 0.43 6.97

1.39 1.22 38.5

38.5

Table 5. Crystalline index

Means were for 4 samples

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Mank

A. *brasiliensis*

decayed

067.58

70.04

63.2

63.6

67.7

67.7

Table 6. SEM/EDAX composition of wood and W/DGEBA/EO/RAMA samples

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 $\text{CH}_3\text{COOH} + \text{H}_2\text{O}_2 \; \overset{\text{H}^+}{\xrightarrow{\hspace*{0.5cm}}} \; \text{CH}_3\text{COOOH} + \text{H}_2\text{O}$ per acetic acid acetic acid $\text{CH}_{2} \text{O} \text{C} \text{C} \text{H}_{2} \gamma \text{C} \text{H} \text{C} \text{H} \text{C} \text{H} \text{C} \text{H} \text{C} \text{H}_{2} \text{C} \text{H} \text{C} \text{H}_{2} \text{C} \text{H}_{2} \text{C} \text{H}_{2} \text{C} \text{H}_{2} \text{C} \text{H}_{3} \text{C} \text{H}_{4} \text{C} \text{H}_{5} \text{C} \text{H}_{6} \text{C} \text{H}_{7} \text{C} \text{H}_{8} \text{C} \text$ CH_2-OC (CH_2) $CH = CH - CH_2$ $CH = CH - CH_2$ $-CH = CH - CH_2$ $-CH_3$ $\frac{\partial \phi}{\partial x} \frac{\partial}{\partial x} \frac{\partial}{\partial y} \frac{\partial}{\partial y} = \frac{\partial \phi}{\partial x} - \frac{\partial \phi}{\partial y} - \frac{\partial \phi}{\partial y} + \frac{\partial \phi}{\partial y} - \frac{\partial \phi}{\partial y} + \frac{\partial \phi}{\partial y} - \frac{\partial \phi}{\partial y} - \frac{\partial \phi}{\partial y} + \frac{\partial \phi}{\partial y} - \frac{\partial \phi}{\partial y} + \frac{\partial \phi}{\partial y} - \frac{\partial \phi}{\partial y} + \frac{\partial \phi}{\partial y} + \frac{\partial \phi}{\partial y} + \frac{\partial \phi}{\partial y} + \$

- New synthetic and natural epoxy derivatives as wood coatings were obtained.
- The epoxy derivatives were thermally crosslinked.
- The influence of coating on wood thermal stability and fungi resistance was made.

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