



# Synthesis of a novel phosphorus-nitrogen flame retardant and its application in epoxy resin



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## ABSTRACT

A novel phosphorus-nitrogen flame retardant named as melamine phenyl phosphate (MAPPO) was synthesized successfully via the neutralization reaction between phenylphosphonic acid (PPOA) and melamine (MA). The chemical structure of MAPPO was characterized by Fourier transform infrared spectra (FT-IR), nuclear magnetic resonance (NMR) and element analysis (EA). MAPPO was introduced into epoxy resin by blending to improve the flame retardancy. Flame retardancy and combustion behavior of EP/MAPPO were investigated by limiting oxygen index (LOI) test, vertical burning (UL-94) test and cone calorimeter test. UL-94 and LOI tests results showed EP containing 18 wt% MAPPO passed the UL-94 V-0 rating and got a high LOI value of 33%. In the cone calorimeter test, compared with that of EP, the values of peak of heat release rate (HRR), total heat release (THR), peak of smoke production rate (PSPR) and total smoke production (TSP) of modified EP were reduced by 58.7%, 40%, 49% and 61.6%, respectively. By analyzing the volatile pyrolysis products of MAPPO, it was known that MAPPO mainly produced CO<sub>2</sub>, NH<sub>3</sub>, H<sub>2</sub>O and other nitrogen-containing compounds, which diluted the concentration of fuel gases and oxygen during combustion. Meanwhile, the char residue of EP/MAPPO system after combustion was also analyzed by scanning electron microscope (SEM), FT-IR and Raman tests, and the results showed MAPPO was able to promote the crosslinking of EP leading to the formation of compact char layer containing P–O–C, P=O and C=C, etc. In a word, the enhancement in flame retardancy was attributed to both dilution effect of non-combustible gases and barrier effect of compact char.

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## 1. Introduction

As one of the most common used thermoset polymers, epoxy resins are widely used in the fields of adhesives, coatings, aerospace & aviation, composites and electronic circuit board because of its good adhesive property, excellent dimensional stability, high mechanical strength, outstanding chemical resistance and excellent dielectric performance [1–6]. However, the inherent flammability and lots of smoke production defects of epoxy resin (EP) which seriously restricts its application in many fields to a certain extent.

For the current industrial products, adding a small amount of halogen-containing flame retardants is a normal way to improve the flame retardancy of EP, but halogen-containing EP composites

will produce some toxic or smoke during combustion, which leads to the harms to the environment and human safety as well [7,8]. Hence, it is necessary to develop the efficient and environmentally friendly flame retardants to replace halogen-containing one for solving the above problems.

To date, a variety of halogen-free flame retardants have been developed to improve the fire retardancy of EP, including inorganic hydroxides [9–11], organic phosphorus-containing flame retardants [12–16] and intumescent fire retardants (IFR) [17–19]. Due to low flame-retardant efficiency, high loading of inorganic hydroxides are always required, which compromise to the mechanical properties. Although organic phosphorus-containing flame retardants can endow satisfied flame retardancy of EP, their smoke production has not been well inhibited. For example, Xu et al. [20] prepared a novel DOPO-based curing agent (IHODOPO) derived from DOPO and imidazole for EP, and fire tests results presented that EP containing 15 wt% IHODOPO can pass the UL-94

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V-0 rating and achieved a LOI value of 37%, while the smoke production was increased compared with that of neat EP. Intumescent flame retardant (IFR) is considered to be a promising method for imparting EP with expected flame retardancy, more importantly, which can effectively achieve smoke suppression effect due to its condensed phase activity [21–24]. Basically, IFR consists of an acid source, a charring agent and a gas source. Once the material containing IFR is ignited, the intumescent char structure can be developed through the dehydration, charring and foaming process, which restrains the heat and oxygen transfer, thereby improving the flame retardancy and smoke suppression. For non-charring resins, IFR/resin system can be constructed with above three components, while only the acid source and gas source are required to prepare IFR/EP system because of the good charring ability of EP. In most cases, some phosphorous-nitrogen containing flame retardants, such as melamine cyanurate (MCA), melamine phosphate (MP), melamine polyphosphate (MPP) and ammonium polyphosphate (APP) can provide the acid source and gas source for IFR/EP system [25–28]. By the comparison with the previous three flame retardants, APP possesses a relatively high flame-retardant efficiency, but adding 20 wt% APP still can not make EP pass V-0 rating [29]. In addition, the poor compatibility between inorganic IFRs (MCA, MP, MPP and APP) with EP matrix also resulted in the decrease of flame retardancy.

To address some of above problems, a novel organic melamine phosphonate intumescent flame retardant was synthesized by the neutralization reaction between phenylphosphonic acid (PPOA) and melamine (MA) for EP. A series of flame-retardant EP was obtained by introducing different amount of MAPPO. Thermal stabilities and charring abilities of MAPPO and EP/MAPPO samples were investigated by TG. Fire retardancy and combustion behavior of EP and EP/MAPPO samples were investigated by LOI, UL-94 and cone calorimeter tests. Besides, the flame-retardant mechanism of MAPPO was also studied by TG-IR, SEM, FT-IR and Raman tests.

## 2. Experimental

### 2.1. Materials

Diglycidyl ether of bisphenol A (DGEBA, E-44) was obtained by Nantong Xingchen Synthetic Material Co., Ltd. (Nantong, China). 4, 4'- Diamino diphenylmethane (DDM) and melamine (MA) were purchased from Sinopharm Chemical Reagent Co., Ltd. (Shanghai, China). Phenylphosphonic acid (PPOA) was purchased from Aladdin Chemistry Co., Ltd. (China). Distilled water was obtained by our Lab.

### 2.2. Synthesis of flame retardant melamine phenyl phosphate (MAPPO)

Route for synthesis of MAPPO was shown in Scheme 1. Firstly, phenylphosphonic acid (7.9 g, 0.05 mol) and 200 mL deionized water were added into a 500 mL three-neck flask equipped with a mechanical stirrer and reflux condenser. Then the mixture was heated to 100 °C with continuous stirring. After that, melamine

(12.6 g, 0.1 mol) was added to flask by twice in 20 min. After finishing, the solution was kept stirring for 5 h. Finally, the reaction solution was cooled slowly to room temperature. The products was filtered and washed by ethanol several times, and then dried under vacuum at 80 °C for 12 h to obtain the white product (yield: 98%).

### 2.3. Synthesis of cured epoxy resins

Formulas of cured epoxy resin samples were listed in Table 1. The preparation process of cured epoxy resins modified with MAPPO was follows: DGEBA and MAPPO were mixed together with a magnetic stirring at 100 °C for 30 min until a homogenous mixture was obtained. After that, DDM was poured into the above mixture, and was kept stirring for 2–3 min. Finally, the mixture was rapidly charged into mold, and cured at 100 °C for 2 h and 150 °C for 3 h. The EP was also prepared by the same procedure without MAPPO.

### 2.4. Measurements

Fourier transform infrared spectra (FT-IR) of samples were obtained using a Nicolet 6700 infrared spectrometer in the range of 4000–400  $\text{cm}^{-1}$  at rt. The powder samples were mixed with KBr powders and pressed into tablets.

$^1\text{H}$  and  $^{31}\text{P}$  nuclear magnetic resonance (NMR) spectra of samples were recorded on a Bruker Ascend 400 spectrometer using DMSO as the solvent.

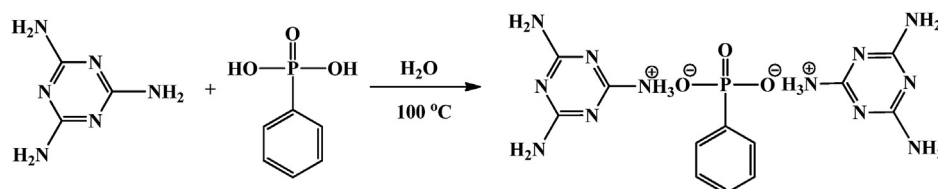
Thermogravimetry analysis (TG) test performed on thermogravimetric analyzer (TGA4000, USA). About 8 mg samples (MAPPO powder and cured EP resin pellets) were putted in alumina crucible and heated from 40 °C to 700 °C at a heating rate of 10 °C/min under nitrogen. In addition, the gases produced from thermal decomposition process from 40 to 700 °C at a heating rate of 10 °C/min were analyzed by FT-IR coupled with TG.

Differential scanning calorimeter (DSC) spectra were connected with a PE DSC 4000 at a heating rate of 10 °C/min from 40 °C to 200 °C under nitrogen flow of 50 mL/min.

LOI values were obtained using a HC-2C oxygen index instrument (Jiangning, China) according to ASTM D2863-97, with sheet sizes of 130 × 6.5 × 3.2 mm. UL-94 rating test was measured on a CZF-4 instrument (Jiangning, China) according to ASTM D3801, and the size of sheets was 130 × 13 × 3.2 mm. Cone calorimeter test was measured using a cone calorimeter (Fire Testing Technology, UK) according to ISO5660-1 at a heat radiant flux of 35  $\text{kW/m}^2$ , and the size of each sample was 100 × 100 × 3.2 mm.

**Table 1**  
LOI and UL-94 results of EP and EP/MAPPO samples.

Sample	DGEBA (%)	DDM (%)	MAPPO (%)	UL-94	LOI (%)
EP	80	20	0	NR	25.6 ± 0.5
EP/5MAPPO	76	19	5	NR	32.2 ± 0.5
EP/10MAPPO	72	18	10	V-1	33.3 ± 0.5
EP/15MAPPO	68	17	15	V-1	34.0 ± 0.5
EP/18MAPPO	65.6	16.4	18	V-0	33.0 ± 0.5



**Scheme 1.** Route for synthesis of MAPPO.

The micromorphology of chars after cone calorimeter test was observed using a JEOL JSM-5900LV scanning electron microscopy (SEM) instrument in a high vacuum at a voltage of 20 kV.

The LabRAM HR800 laser Raman spectrometer (SPEX Co.) was carried out to analyze the char structure with a 532 nm helium-neon laser line at room temperature.

### 3. Results and discussion

#### 3.1. Characterization of MAPPO

The structure of MAPPO was firstly characterized by FT-IR, Fig. 1 showed the IR spectra of PPOA, MA and MAPPO. For PPOA, three characteristic peaks at  $2732\text{ cm}^{-1}$ ,  $1438\text{ cm}^{-1}$  and  $1149\text{ cm}^{-1}$  were observed, which belonged to P–OH, benzene ring and P=O groups, respectively. For MA, the peaks at  $3468\text{ cm}^{-1}$ ,  $3418\text{ cm}^{-1}$ ,  $3331\text{ cm}^{-1}$  and  $3123\text{ cm}^{-1}$  were attributed to different  $\text{NH}_2$ - bonds of MA [30]. The peak at  $1650\text{ cm}^{-1}$  was assigned to C=N bond. For MAPPO, by comparison with MA, both the change of the position of C=N which moved from  $1650$  to  $1676\text{ cm}^{-1}$  and the appearance of P=O bond, suggesting PPOA was successfully attached to the molecule of MA [31].

The structure of MAPPO was further confirmed by NMR test. In Fig. 2(a), compared with PPOA, the new peak appeared at 6.7 ppm, which was assigned to  $\text{NH}_2$ - groups of MA. Meanwhile, the ratio of integrated areas of a: b: c was 2: 3: 12, which was in accordance with the number ratio of corresponding hydrogen protons in MAPPO. Moreover, Fig. 2 (b) presented the  $^{31}\text{P}$  NMR of PPOA and MAPPO. In Fig. 2(b), the position of P atom of PPOA at 12.79 ppm, while the position of P atom of MAPPO moved to 11.23 ppm since the electron cloud of both oxygen anion was dispersed by the ionic bond after salt formation. The results of IR and NMR implied that the target product MAPPO was successfully prepared. Table 2 showed the elemental contents of MAPPO. As seen in Table 2, the experimental value of C, H and N were approximately equal to calculated value. The above results confirmed that the target product (MAPPO) was successfully prepared.

Thermal decomposition behavior of MAPPO was also investigated by TG test, Fig. 3 showed the TGA and DTG curves of MAPPO. As seen, the onset decomposition temperature ( $T_{5\%}$ , defined as the temperature at which 5 wt% mass loss) of MAPPO was  $264.5\text{ }^\circ\text{C}$ , and presented mainly four stage decompositions with 16 wt% residual mass at  $700\text{ }^\circ\text{C}$ . The temperature at the maximum mass loss rate ( $T_{\text{max}}$ ) of MAPPO was  $287\text{ }^\circ\text{C}$ ,  $360\text{ }^\circ\text{C}$ ,  $515$  and  $620\text{ }^\circ\text{C}$ , respectively. To further analyze the gaseous product released in heating process,

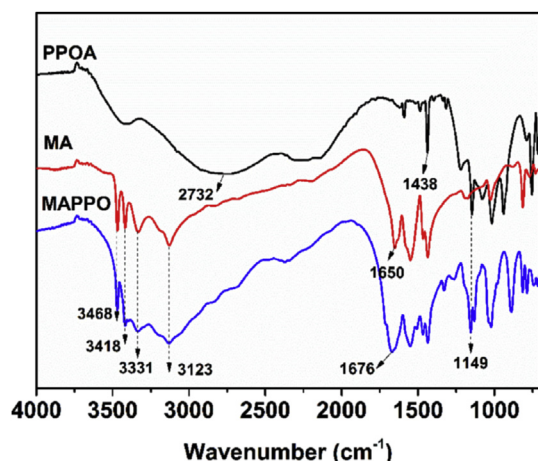


Fig. 1. IR spectra of PPOA, MA and MAPPO.

TG-IR test was carried out. As seen in Fig. 4, the main gaseous products at the temperature range from  $250\text{ }^\circ\text{C}$  to  $450\text{ }^\circ\text{C}$  were  $\text{CO}_2$  and  $\text{H}_2\text{O}$ , which was mainly caused by the breaking of a part of C–N, the dehydrogenation of melamine and the dehydration phosphoric-containing acid [29]. As the temperature increased from  $450\text{ }^\circ\text{C}$  to  $600\text{ }^\circ\text{C}$ , MAPPO produced  $\text{NH}_3$  ( $965, 932\text{ cm}^{-1}$ ),  $-\text{OH}$  ( $3547\text{ cm}^{-1}$ ), C=N ( $1558\text{ cm}^{-1}$ ), C≡N ( $2245\text{ cm}^{-1}$ ) [31,32], amines and aromatic compounds ( $3091\text{ cm}^{-1}$ ), which was attributed to the ring-opening reactions of triazine and benzene rings [33].

#### 3.2. Flame retardancy and combustion behavior

Flame retardancy of EP and flame-retardant EP was investigated by LOI and UL-94 tests. As seen in Table 1, EP was flammable with a LOI value of 25.6% and failed to UL-94 test. Adding 10 wt% MAPPO allowed EP/10MAPPO to pass UL-94 V-1 rating. Further increasing the content of MAPPO to 18 wt%, the EP/18MAPPO successfully reached V-0 rating. For LOI tests, after adding 5 wt% MAPPO, the LOI value of EP/5MAPPO achieved 32%. However, with the increasing addition of MAPPO, the LOI value of EP/MAPPO increased slightly, and EP/15MAPPO had a highest LOI value of 34%. It suggested that the phosphorus component of MAPPO was mainly worked in the condensed phase, and the fuel dilution effects of ammonia gas was inefficient at high oxygen concentration atmosphere [22,34].

Cone calorimeter test is an effective bench scale way to evaluate the combustion behavior of materials, which provides many important parameters including the time to ignition (TTI), peak of heat release rate (PHRR), time to PHRR ( $t_p$ ), total heat release (THR), peak of smoke production rate (PSPR), total smoke production (TSP), total smoke release (TSR), average CO yield (av-COY), average rate of heat emission (ARHE), average effective heat of combustion (av-EHC) and char residues, etc. Fig. 5 presented the curves of HRR, THR, ARHE and TSP, and corresponding data were listed in Table 3.

As seen in Fig. 5 (a), EP had a high PHRR value of  $1073\text{ kW/m}^2$ , while the HRR value of EP/18MAPPO decreased to  $443\text{ kW/m}^2$  with a reduction of 58.7%, which was caused by rapid char formation and fuel dilution of non-combustible gases produced by MAPPO in advance [29]. The pictures of char residues were shown in Fig. 6, epoxy resin almost burned out, while EP/18MAPPO showed a strongly expanded carbon residue with a residual mass of up to 31.6%, which served as a good barrier to insulate the transfer of heat and oxygen and proved the existence of condensed phase activity during combustion [35]. A large amount of decomposition products of EP were participated in charring instead of burning, resulting in the direct reduction of fuel and soot particles which were incomplete combustion. As seen in Table 3, it was clear that the peak of smoke production rate (PSPR) and total smoke production (TSP) of EP/18MAPPO were remarkable reduced compared with those of EP, which were reduced by 49% and 61.6% respectively. Because of the good inhibition function of the combustion, the THR value of EP/18MAPPO decreased by 40% as well. However, the value of EHC, which related to the burning degree of volatile gases in gaseous phase during combustion, was slightly decreased by 8.5%, and the CO yield was no significant change with MAPPO addition. This result suggested that there was few fragments with free radical trapping formed in the gaseous phase, and the fuel-dilution by non-flammable gas such as  $\text{NH}_3$ ,  $\text{H}_2\text{O}$  was the major flame-retardant mechanism in gaseous phase. In addition, to further evaluate the fire safety of epoxy resin, fire growth rate (FIGRA, defined as the maximum value of  $\text{HRR}/t$  and was always equal to  $\text{PHRR}/t_p$ ) and maximum average rate of heat emission (MARHE, defined as the maximum value of  $\text{THR}(t)/t$  where  $t$  was the testing time) were also calculated. Compared with EP, the FIGRA and MARHE values of EP/18MAPPO were largely decreased, demonstrating adding MAPPO was able to slow down the combustion rate, and improve the flame



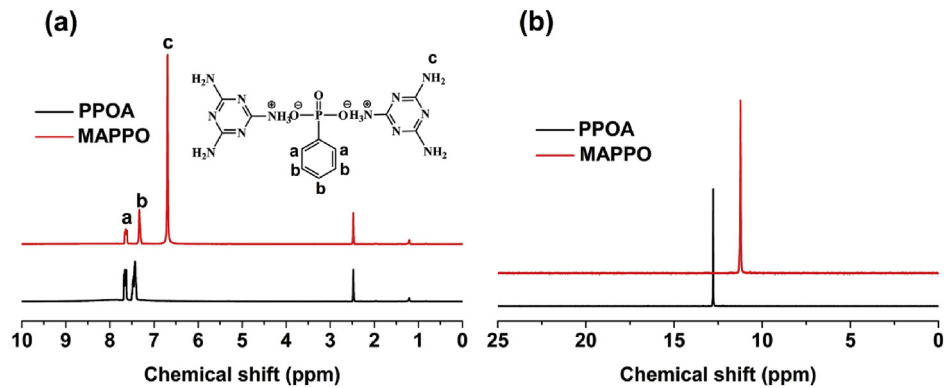


Fig. 2.  $^1\text{H}$ NMR (a) and  $^{31}\text{P}$ NMR (b) spectra of PPOA and MAPPO.

Table 2  
Elemental contents of MAPPO.

Sample	Cal. (wt%)			Exp. (wt%)		
	C	H	N	C	H	N
MAPPO	35.12	4.67	40.96	34.62	4.53	41.42

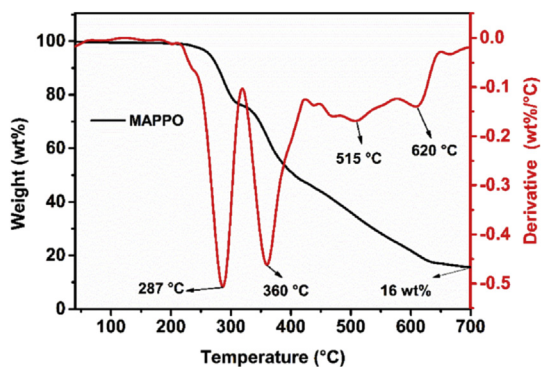


Fig. 3. TG and DTG curves of MAPPO under  $\text{N}_2$ .

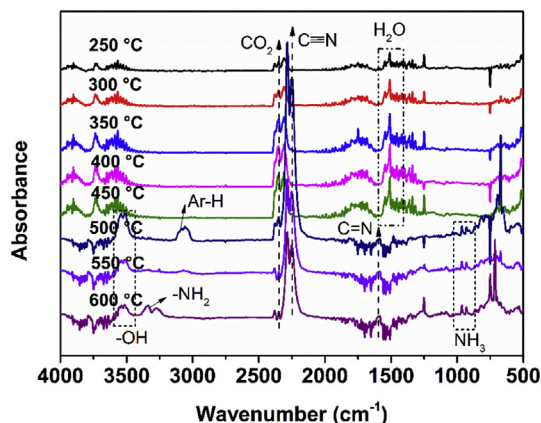


Fig. 4. TG-FTIR spectra of the pyrolysis products of MAPPO at different temperature.

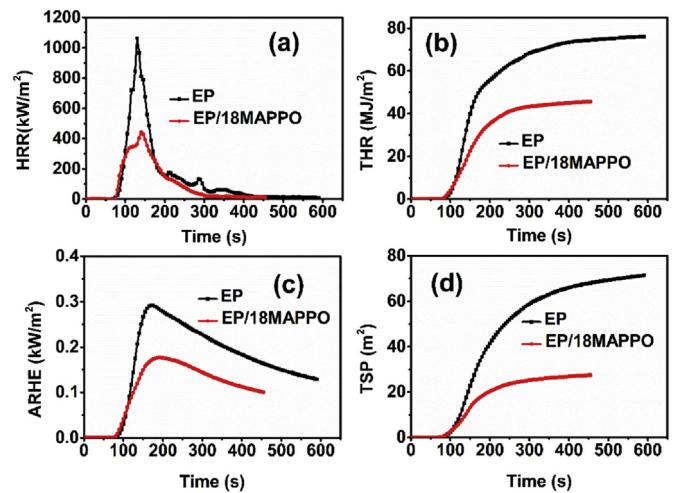


Fig. 5. The curves of HRR (a), THR (b), ARHE (c) and TSP (d) of EP and EP/18MAPPO after cone calorimeter test.

Table 3  
Cone calorimeter data of EP and EP/18MAPPO.

Sample	EP	EP/18MAPPO
TTI (s)	60 ± 1	68 ± 2
$t_p$ (s)	130 ± 3	140 ± 4
PHRR ( $\text{kW}/\text{m}^2$ )	1073 ± 55	443 ± 20
FIGRA ( $\text{kW}/\text{m}^2 \cdot \text{s}$ )	8.3	3.2
THR ( $\text{MJ}/\text{m}^2$ )	76 ± 3	46 ± 2
MARHE ( $\text{kW}/\text{m}^2$ )	291.6	176.9
PSPR ( $\text{m}^2/\text{s}$ )	0.55 ± 0.02	0.28 ± 0.01
TSP ( $\text{m}^2$ )	71.4 ± 3	27.4 ± 1
TSR ( $\text{m}^2/\text{m}^2$ )	5241 ± 400	3015 ± 200
av-COY	0.095 ± 0.01	0.094 ± 0.01
av-EHC	21.1 ± 1	19.3 ± 1
Char residue (wt %)	10.2 ± 0.5	31.6 ± 1.5

retardancy of EP [36,37].

### 3.3. Thermal behavior analysis

Glass transition temperature ( $T_g$ ) of EP and flame-retardant EP was investigated by DSC, and the corresponding data shown in Fig. 7. From Fig. 7, all samples showed a single  $T_g$ , and the EP possesses the highest  $T_g$  value of 159 °C. With the addition of MAPPO, the  $T_g$  value of EP/MAPPO samples was decreased gradually. This was mainly due to the large free volume and stereo-hindrance of

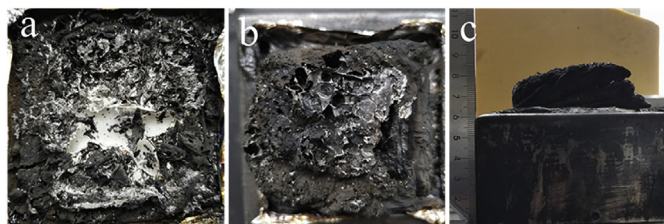


Fig. 6. Digital photos of char residues for EP (a), EP/18MAPPO (b,c) after cone calorimeter test.

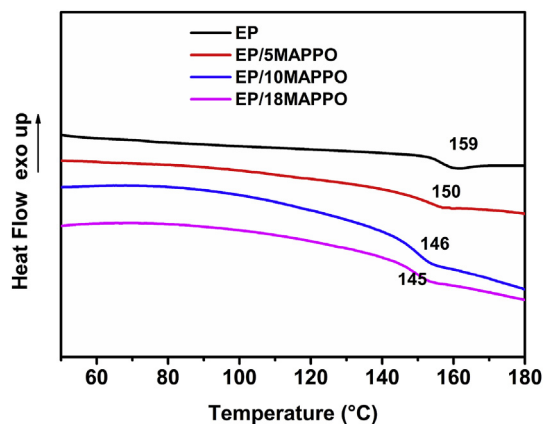


Fig. 7. DSC curves of EP and EP/MAPPO samples.

MAPPO, resulting in the decrease of the crosslinking degree of the EP/MAPPO system [38].

Fig. 8 showed the TGA and DTG curves of MAPPO, and corresponding data were collected in Table 4. For EP, it began to decompose at 355.8 °C ( $T_{5\%}$ ) and showed one-step decomposition with a maximum weight mass loss rate at 380.5 °C and a residual mass of 20.2 wt%. The thermal decomposition of EP at 380.5 °C

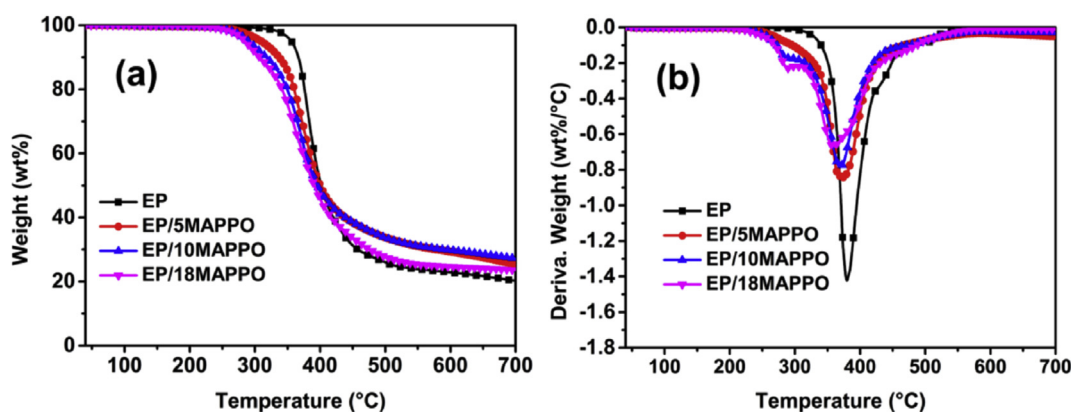


Fig. 8. TGA (a) and DTG (b) curves of EP and flame-retardant EP/MAPPO samples.

Table 4

TGA and DTG data of MAPPO, EP and EP/MAPPO samples.

Sample	$T_{5\%}$ (°C)	$T_{max}$ (°C)	Rate at $T_{max}$ (%/min)	Residue at 700 °C (wt%)
EP	355.8	380.5	1.4	20.2
EP/5MAPPO	309.5	372.7	0.84	25.2
EP/10MAPPO	290.1	369.2	0.78	27.1
EP/18MAPPO	285.1	359.2	0.66	23.6

( $T_{max}$ ) was contributed to the breakage of crosslinked molecular chain of EP itself [39]. For EP/MAPPO samples, the  $T_{5\%}$  and  $T_{max}$  decreased gradually with the increase of the addition amount of MAPPO, which was caused by the early decomposition of MAPPO. However, the residual mass of EP/MAPPO samples at 700 °C was higher than that of EP, and the rate at  $T_{max}$  of all EP/MAPPO samples was reduced. The reason was that MAPPO decomposed in advance to produce some phosphoric-containing acid, acting as dehydrating agents to catalyze the degradation and carbonization of EP.

### 3.4. Flame-retardant mechanism

To investigate the condensed phase mechanism of EP/MAPPO system, char residues after cone calorimeter test were analyzed by SEM, IR and Raman. As seen in Fig. 9, the char layer of EP was rough and had many apparent crevices. Compared with EP, the char layer of EP/18MAPPO was relatively smooth and compact, suggesting that MAPPO was able to improve the quality of char residue during combustion.

The element composition of the char residues were investigated by EDX, and the relevant data were listed in Table 5. It was found that the composition of phosphorus in the char residue of EP/18MAPPO was higher than the theoretical value of phosphorus content added into the cured EP/18MAPPO (1.36 wt%), which indicated phosphorus derived from MAPPO mainly left in the char residue as well.

Raman spectroscopy was considered to be an effective method for measuring the order degree of carbon residues and corresponding data were shown in Fig. 10. Two peaks at 1358  $\text{cm}^{-1}$  and 1560  $\text{cm}^{-1}$  were observed in Fig. 10, which were assigned to D and G bonds, respectively. Generally, the D bond was owing to disordered graphite or glassy carbon, and the G bond belonged to vibration of  $\text{sp}^2$ -hybridized aromatic layers. Basically, R value equaled to the  $I_D/I_G$  (defined as intensities ratio of D bond to G bond) which was assessed the degree of graphitization, and the higher R value meant the lower the graphitization degree [40]. As seen, the R value of EP/18MAPPO (3.34) was lower than that of EP (4.03), implying the char layer of EP/18MAPPO with graphitization structure play a

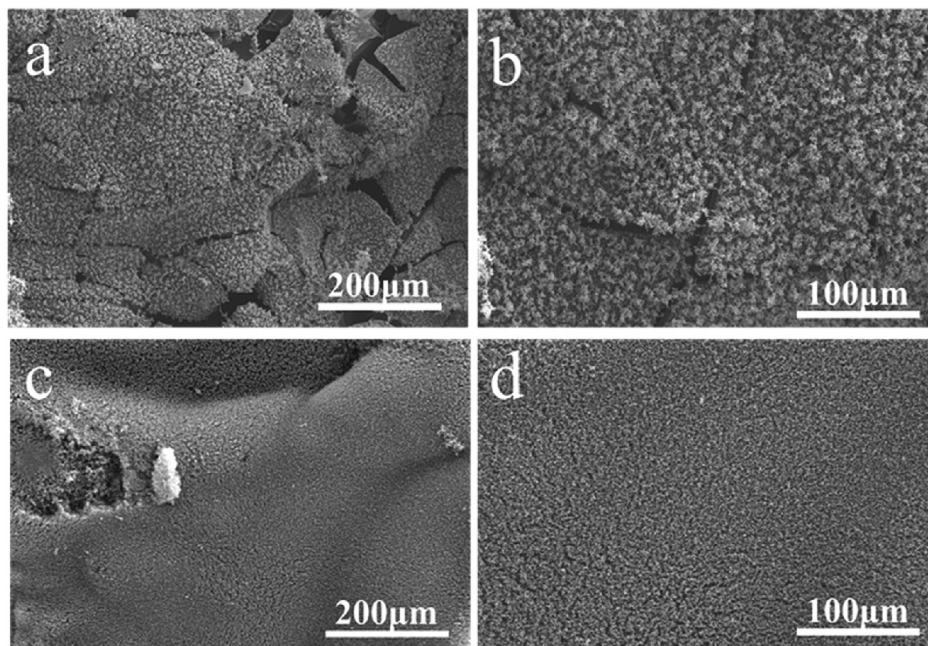


Fig. 9. SEM images of char residues for EP (a, b) and EP/18MAPPO (c, d).

better role in the insulation of heat and oxygen.

The concentration of char residues was further analyzed by IR. In Fig. 11, the absorption peaks at about  $3000\text{ cm}^{-1}$  and  $1609\text{ cm}^{-1}$  were assigned to  $\text{CH}_2$ - and  $\text{C}=\text{C}$  bonds, respectively. However, some differences were found in EP/18MAPPO. The peaks at  $1231\text{ cm}^{-1}$  and  $1176\text{ cm}^{-1}$  belong to  $\text{P}=\text{O}$  and  $\text{P}-\text{O}-\text{C}$  bonds, respectively, demonstrating some organophosphorus compounds existed in char residues after burning [41]. The above results proved that some compounds produced by MAPPO accelerated the cross-linking of EP degradation products to form some stable and compact char residues rich in organophosphorus compounds.

Based on the above analysis, the flame-retardant mechanism of EP/MAPPO system was concluded as follows. In the gaseous phase, MAPPO generated a large of nonflammable gases, such as  $\text{NH}_3$ ,  $\text{CO}_2$  and  $\text{H}_2\text{O}$ , which diluted oxygen and fuel gases produced by decomposition of epoxy resin as well as took away the heat during combustion. In the condensed phase, the poly-/pyro-/

ultraphosphoric acids generated from degradation of MAPPO would react with epoxy resin through the dehydration and carbonization. Large amount of EP molecular fragments remained in the condensed phase to promote the formation of expanded char layer with  $\text{P}-\text{O}-\text{C}$  structure. This expanded char layer was able to serve as a good barrier to restrict the heat and oxygen transfer. Consequently, the enhancement in flame retardancy was attributed to the diluting effect of nonflammable gases and the barrier effect of expanded char residues with  $\text{P}-\text{O}-\text{C}$  structure at the same time.

#### 4. Conclusions

In this paper, a novel phosphorus-nitrogen flame retardant named as MAPPO was synthesized successfully by the neutralization reaction and used to improve the flame retardancy of EP. As expect, by incorporation of 18 wt% MAPPO, epoxy resin not only passed the UL-94 V-0 rating and achieved a high LOI value of 33%, but also significantly suppressed the heat release and smoke

Table 5  
Element composition of the char residues for EP/18MAPPO after combustion.

Sample	C (wt%)	O (wt%)	N (wt%)	P (wt%)
EP/18MAPPO	80.2	11.3	4.8	3.7

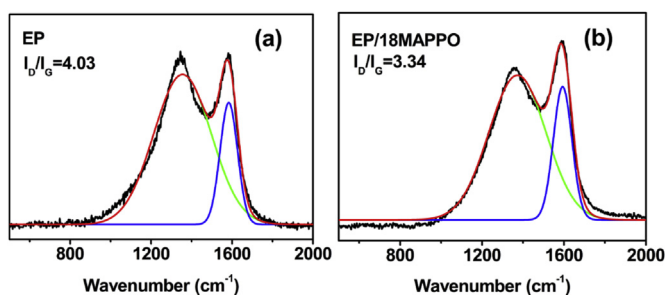


Fig. 10. Raman spectra of char residues for EP (a) and EP/18MAPPO (b).

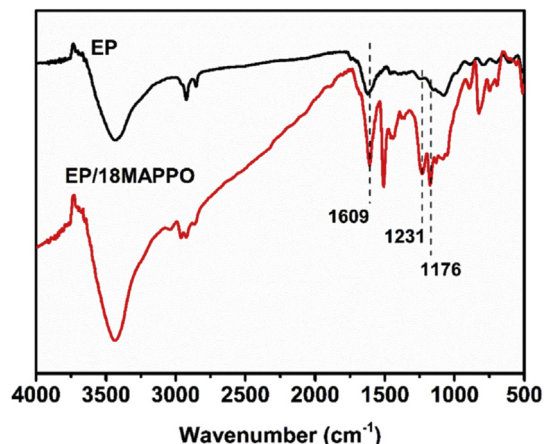


Fig. 11. IR spectra of char residues for EP and EP/18MAPPO.



production. By the analysis of TG-IR, SEM, IR and Raman, it gave a clear conclusion that the improvement in flame retardancy was contributed to both gaseous and condensed phase. In gaseous phase, some non-flammable gases such as NH<sub>3</sub>, CO<sub>2</sub> and H<sub>2</sub>O diluted the concentration of oxygen and fuel gases to slow down the combustion. In condensed phase, phosphorus-containing acids produced in high temperature would react with epoxy resin by dehydration and carbonization to form a stable and compact char layer, which was used as a good protective layer to interrupt the combustion.

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